

CarTech® 718 Alloy

	Identification	
UNS Number		
• N07718		
DIN Number		

• 2.4668

Type Analysis							
Single figures are nominal except	where noted.						
Carbon (Maximum)	0.08 %	Manganese (Maximum)	0.35 %				
Phosphorus (Maximum)	0.015 %	Sulfur (Maximum)	0.015 %				
Silicon (Maximum)	0.35 %	Chromium	17.00 to 21.00 %				
Molybdenum	2.80 to 3.30 %	Copper (Maximum)	0.15 %				
Cobalt (Maximum)	1.00 %	Titanium	0.65 to 1.15 %				
Aluminum	0.35 to 0.80 %	Columbium + Tantalum	4.75 to 5.50 %				
Boron	0.001 to 0.006 %	Nickel + Cobalt	50.00 to 55.00 %				
Iron	Balance						

The Cobalt content is on an "If determined" basis.

General Information

Description

CarTech 718 alloy is a precipitation hardenable nickel-base alloy designed to display exceptionally high yield, tensile and creep-rupture properties at temperatures up to 1300°F (704°C). The sluggish age-hardening response of CarTech 718 permits annealing and welding without spontaneous hardening during heating and cooling. This alloy has excellent weldability when compared to the nickel-base superalloys hardened by aluminum and titanium.

Applications

This alloy has been used for jet engine and high-speed airframe parts such as wheels, buckets, spacers, and high temperature bolts and fasteners. It has also been used extensively in oil and gas drilling and production due to its high strength and resistance to chlorides, stress corrosion and sulfide stress cracking. Within the oil and gas industry, this alloy has been used in valves, tubing hangers, MWD/LWD parts, fishing tools, pump shafts and wellhead components.

Corrosion Resistance

Important Note: The following 4-level rating scale is intended for comparative purposes only. Corrosion testing is recommended; factors which affect corrosion resistance include temperature, concentration, pH, impurities, aeration, velocity, crevices, deposits, metallurgical condition, stress, surface finish and dissimilar metal contact.

Nitric Acid	Good	Sulfuric Acid	Moderate
Phosphoric Acid	Moderate	Acetic Acid	Good
Sodium Hydroxide	Good	Salt Spray (NaCl)	Excellent
Sea Water	Moderate	Sour Oil/Gas	Good
Humidity	Excellent		

	Properties
Physical Properties	
Density	0.2970 lb/in³

CarTech® 718 Alloy

Mean CTE	
77 to 200°F	7.10 x 10 ∘ in/in/°F
77 to 400°F	7.50 x 10 ∘ in/in/°F
77 to 600°F	7.70 x 10 ∘ in/in/°F
77 to 800°F	7.90 x 10 ∘ in/in/°F
77 to 1000°F	8.00 x 10 ∘ in/in/°F
77 to 1200°F	8.40 x 10 ∘ in/in/°F
77 to 1400°F	8.90 x 10 ∘ in/in/°F

Coefficient of Thermal Expansion

Temperatu	ıre Range	10 ⁻⁶ /°F	10-⁵/°C	
77°F to	25°C to	107-6	10-7-0	
200	93	7.1	12.8	
400	204	7.5	13.5	
600	316	7.7	13.9	
800	427	7.9	14.2	
1000	538	8.0	14.4	
1200	649	8.4	15.1	
1400	760	8.9	16.0	

Modulus of Elasticity (E)	
70°F	29.6 x 10 ₃ ksi
200°F	29.2 x 10 ₃ ksi
400°F	28.8 x 10 ³ ksi
600°F	27.6 x 10 ³ ksi
800°F	26.5 x 10 ₃ ksi
1000°F	25.5 x 10 ₃ ksi
1200°F	24.5 x 10 ₃ ksi
1400°F	23.1 x 10 ³ ksi
1600°F	18.1 x 10 ₃ ksi
1750°F	11.1 x 10 ₃ ksi

Modulus of Elasticity (E)

Temp	erature			
°F	°C	psi x 10 ⁶	MPa x 10 ³	
70	21	29.6	204	
200	93	29.2	201	
400	204	28.8	199	
600	316	27.6	190	
800	427	26.5	183	
1000	538	25.5	176	
1200	649	24.5	169	
1400	760	23.1	159	
1600	871	18.1	125	
1750	954	11.1	76.5	

Electrical Resistivity (70°F) 728.0 ohm-cir-mil/ft

Melting Range 2200 to 2450 °F

Typical Mechanical Properties

Effect of Solution Treating Temperature on Transverse Room Temperature Properties - Pyromet Alloy 718

Tensile properties of a 4" (101.6 mm) square billet

Solution Treating Temperature		0.2% Yield Strength			rength Elongation Reduction Reckwell		Rockwell C	ASTM Grain	
°F	°C	ksi	MPa	ksi	MPa	in 2" (50.8 mm) of Area		Hardness	Size
1750	954	160.1	1104	183.7	1267	8.1	13.6	42	7
1900	1038	163.7	1129	183.7	1267	12.8	20.3	42	5/6
1950	1066	158.2	1091	180.9	1247	14.0	19.6	42	4/5
2000 2050	1093 1121	154.6 149.9	1066 1033	178.0 171.1		17.3 17.5	24.5 27.9	40 39	4/4.5 3.5/4

Note: All samples solution treated 2 hours at the temperature indicated and air cooled. Aging consisted of 8 hours at 1325°F (718°C), cooled 100°F/hr to 1150°F (56°C/hr to 621°C), held 8 hours at 1150°F (621°C), and air cooled.

Effect of Solution Treating Temperature on the Transverse Stress Rupture Properties – Pyromet Alloy 718

4" (101.6 mm) square billet

Solution Treating Temperature		Test Temperature		Str	ess	Rupture Life	% Elongation	% Reduction	
°F	°C	۰F	°C	ksi	MPa	Hours	in 2" (50.8 mm)	of Area	
1750 1900 1950 2000	954 1038 1066 1093	1300 1300 1300 1300	704 704 704 704	75 75 75 75	517 517 517 517	64.8 132.1 95.2 141.0	17.4 9.4 7.9 2.5	25.3 17.2 10.8 6.8	

Notes: All samples solution treated 2 hours at the temperatures indicated and air cooled. Aging consisted of 8 hours at 1325°F (718°C), cooled 100°F/hr to 1150°F (56°C/hr to 621°C), held 8 hours at 1150°F (621°C), and air cooled.

All specimens were combination smooth-notch bars with 0.178" (4.52 mm) gage diameter, 0.712" (18.1 mm) gage length and $K_t = 3.8$.

Stress rupture notch sensitivity may result from 1900°F (1038°C) solution treatment. This is due to reduction of precipitate at grain boundaries with this treatment.

Elevated Temperature Tensile Tests - Pyromet Alloy 718 1/2" (12.7 mm) bar stock

Test Temperature			0.2% Yield Strength		sile ngth	% Elongation	
۰F	F °C ksi		MPa	ksi	MPa	2" (50.8 mm)	
70 200 400 600 800 1000 1200 1400	21 93 204 316 427 538 649 760	175 170 163 159 156 155 149	1207 1172 1124 1096 1076 1069 1027 758	210 204 198 195 191 185 168	1448 1407 1365 1344 1317 1276 1158 758	22.0 21.0 20.0 20.0 19.0 18.0 19.0 27.0	

Heat Treatment: 1 hr—1800°F (982°C), air cool + 8 hr—1325°F (718°C), cool 100°F/hr to 1150°F (56°C/hr to 621°C), hold 8 hr, air cool.

Low Temperature Tensile Data - Pyromet Alloy 718

Transverse tests-4" (101.6 mm) square billet

Test No.	Tomporatura				Tensile Strength		% Elongation	% Reduction	
	°F	°F °C		MPa	ksi	MPa	in 2" (50.8 mm)	of Area	
1	Room	Room	157	1082	183.8	1267	18.0	21.6	
2	Room	Room	156	1076	181.3	1250	16.5	23.3	
3	Room	Room	152.5	1051	179.5	1238	19.0	29.1	
4	-423	-253	196.2	1353	250.4	1726	14.0	16.2	
5	-423	-253	200	1379	244.2	1684	13.0	17.5	
6	-423	-253	194.2	1339	241.9	1668	12.0	16.7	

Heat Treatment: 2 hr—1950°F (1066°C), air cool + 8 hr—1325°F (718°C), cool 100°F/hr to 1150°F (56°C/hr to 621°C), hold 8 hr, air cool.

Stress Rupture Data - Pyromet Alloy 718

			Stress for Rupture						
Test Temperature		100 Hours				1000 Hours			
		Smooth		Notch		Smooth		Notch	
°F	°C	ksi	MPa	ksi	MPa	ksi	MPa	ksi	MPa
1100 1200 1300 1400	593 649 704 760	170 110 75 44	1172 758 517 303	220 195 130 63	1517 1344 896 434	130 85 55 25	896 586 379 172	205 170 80 35	1413 1172 552 241

Heat Treatment: 1 hr—1800°F (982°C), air cool +8 hr—1325°F (718°C), furnace cool 100°F/hr to 1150°F (56°C/hr to 621°C), hold 8 hr, air cool.

Heat Treatment

The following heat treatment should be used to obtain the best combination of tensile properties and stress rupture properties:

1 hr 1750°F to 1800°F (954°C to 982°C) air cool + 8 hr 1325°F (718°C) cool 100°F/hr to 1150°F (56°C/hr to 621°C), hold 8 hr and air cool.

To obtain the best room temperature and cryogenic tensile properties, the following heat treatment should be used:

1 to 2 hr 1950°F (1066°C), air cool + 8 hr 1325°F (718°C) cool 100°F/hr to 1150°F (56°C/hr to 621 °C), hold 8 hr and air cool.

Workability

Hot Working

Hot working is carried out using a 2050°F (1121°C) maximum furnace temperature. Hot-cold working in the range 1700/1850°F (927/1010°C) will improve the strength of the forging if the service temperature is below about 1100°F (593°C). Prolonged soaking at the forging temperature is not desirable. The material should be given uniform reductions to avoid the formation of duplex grain structures.

Machinability

The alloy can be readily machined in either the annealed or the age-hardened condition. The age-hardened condition gives better chip action on chip breaker tools and produces a better finish. The annealed condition will give a slightly longer tool life. Tooling and procedures are similar to those used for Carpenter Pyromet alloy X-750.

Weldability

Pyromet alloy 718 can be welded in either the annealed or the aged condition. Welding in the aged condition will cause the formation of a softened heat-affected zone.

Other Information						
Applicable Specifications						
• AMS 5662	• AMS 5663					
• API 6A718	NACE MR0175					
Forms Manufactured						
Bar-Rounds	Bar-Shapes					
• Billet	• Strip					
• Wire	Wire-Rod					

Technical Articles

- A Designer's Manual On Specialty Alloys For Critical Automotive Components
- A Guide to Etching Specialty Alloys for Microstructural Evaluation
- Alloy Selection for Cold Forming (Part I)
- · Alloy Selection for Cold Forming (Part II)
- · Carpenter 286-LNi Alloy A Lower Cost Option for High Temperature Auto and Truck Fasteners
- Forging Difficult Alloys: How to Get Better Results, Consistently
- · How to Select the Right Stainless Steel or High Temperature Alloy for Heading
- · New Requirements for Ferrous-Base Aerospace Alloys
- Selecting High Temperature Alloys for Fasteners in Automotive Exhaust Systems
- · Trends in High Temperature Alloys

Disclaimer:

The information and data presented herein are typical or average values and are not a guarantee of maximum or minimum values. Applications specifically suggested for material described herein are made solely for the purpose of illustration to enable the reader to make his/her own evaluation and are not intended as warranties, either express or implied, of fitness for these or other purposes. There is no representation that the recipient of this literature will receive updated editions as they become available.

Unless otherwise specified, registered trademarks are property of CRS Holdings Inc., a subsidiary of Carpenter Technology Corporation Copyright © 2020 CRS Holdings Inc. All rights reserved.

Visit us on the web at www.cartech.com

Edition Date: 07/15/11