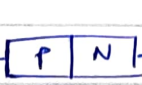


Electronics

Diode (P-N Junction Diode)

- No Bias ($V_D = 0V$) 
- Forward Bias ($V_D > 0V$) 
- Reverse Bias ($V_D < 0$) 

$$I_{D\text{Tot}} = I_{\text{majority}} + I_{\text{minority}}$$

$$= \underset{\text{(mA)}}{I_D} + I_s (\mu A)$$

$$I_D \approx I_s \left(e^{\frac{V_D}{\eta V_T}} - 1 \right)$$

$$\eta = 1 \text{ for Ge}$$

$$\eta = 2, \text{ for Si}$$

I_s = Reverse saturation current

V_D = Diode voltage

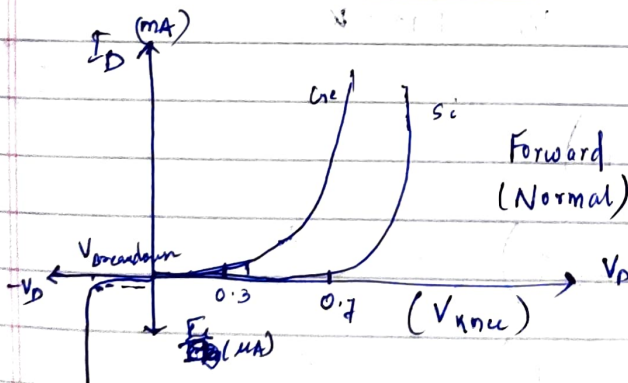
$$V_T = \frac{KT}{q} \quad (\text{Thermal potential})$$

$$K = 1.38 \times 10^{-23} \text{ J/K} \quad \text{Boltzmann const.}$$

$$T = \text{absolute temp} \approx 273^\circ + (^\circ\text{C})$$

$$q = 1.6 \times 10^{-19} \text{ C}$$

V-I characteristics of diode



$$I_D = I_s \left(e^{\frac{V_D}{\eta V_T}} - 1 \right)$$

$$V_D = 0, \quad I_D = 0$$

$$V_D > 0V, \quad I_D = \uparrow$$

$$V_D < 0, \quad I_D \approx -I_s$$

Q. Determine the Germanium p-n junction diode, current for the forward biased voltage of 0.22 V and room temperature 25°C with the temperature reverse saturation current is 1mA .

$$I_D = I_S \left(e^{\frac{V_D}{n V_T}} - 1 \right)$$

$$= 1 \times 10^{-3} \left(e^{\frac{0.22}{1 \times 0.0257}} - 1 \right)$$

$$= 10^{-3} \left(e^{8.56} - 1 \right)$$

$$V_T = \frac{K T}{q}$$

$$= \frac{1.38 \times 10^{-23} \times 298}{1.6 \times 10^{-19}}$$

$$= \frac{1.38 \times 298}{1.6} \times 10^{-4}$$

$$= \frac{412.724}{0.0257} \times 10^{-4}$$

Q. The current voltage of a p-n junction diode is given by Schottky's equation. The diode current is 0.5 mA at $V = 340\text{ mV}$ and 15 mA at $V = 440\text{ mV}$.

The value of $\frac{K T}{q}$ where $\frac{K T}{q} = \frac{25\text{ mV}}{2.5}$

$$I_D = 0.5\text{ mA}$$

$$V_D = 340\text{ mV}$$

$$I_D = 15\text{ mA}$$

$$V_D = 440\text{ mV}$$

$$I_D = I_S \left(e^{\frac{V_D}{n V_T}} - 1 \right)$$

$$\Rightarrow 0.5 = I_S \left(e^{\frac{340}{n \times 25}} - 1 \right) \quad \text{--- (1)}$$

$$\Rightarrow 0.5 = I_S \left(e^{\frac{68}{5n}} - 1 \right) \quad \text{--- (1)}$$

$$\Rightarrow 15 = I_S \left(e^{\frac{440}{n \times 25}} - 1 \right) \quad \text{--- (2)}$$

$$\Rightarrow 15 = I_S \left(e^{\frac{88}{5n}} - 1 \right)$$

$$\frac{0.5}{15} = \frac{e^{\frac{68}{5n}} - 1}{e^{\frac{88}{5n}} - 1}$$

$$\Rightarrow 0.5 \left(e^{\frac{88}{5n}} - 1 \right) = 15 \left(e^{\frac{68}{5n}} - 1 \right)$$

$$\Rightarrow 0.5 e^{\frac{88}{5n}} - 15 e^{\frac{68}{5n}} = -15 + 0.5$$

$$\Rightarrow e^{\frac{88}{5n}} \left(\Rightarrow 0.5 e^{\frac{88}{5n}} = 15 e^{\frac{68}{5n}} \right)$$

$$\Rightarrow \frac{e^{\frac{88}{5n}}}{e^{\frac{68}{5n}}} = \frac{15}{0.5}$$

$$\Rightarrow \frac{e^{\frac{88}{5n} - \frac{68}{5n}}}{1} = \frac{30}{1}$$

$$\Rightarrow \frac{20}{5n} = \log_{10} 30 \Rightarrow \frac{20}{\log_{10} 30} = 5n$$

$$n = \frac{20}{5 \times 3.4} = \frac{20}{17} = 1.176$$

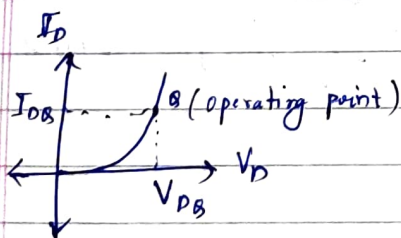
$$\Rightarrow 20 = 5n \log_{10} 30$$

$$\Rightarrow n = \frac{20}{5 \log_{10} 30}$$

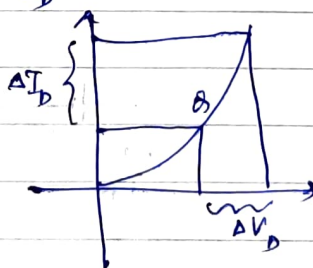
Resistance of Diode

• Static Resistance R_D

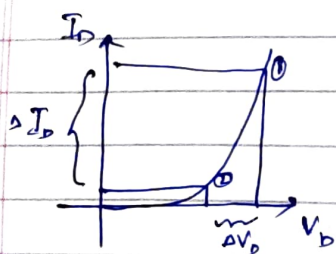
• Dynamic Resistance $\left\{ \begin{array}{l} \text{AC resistance } (r_{ac}) \\ \text{Avg. resistance } (r_{avg}) \end{array} \right.$



$$R_D = \frac{V_{DQ}}{I_{DQ}} \quad \text{at fixed P.T.}$$



$$r_{ac} = \frac{\Delta V_D}{\Delta I_D} = \frac{26 \text{ mV}}{I_D} \quad \text{at fixed P.T.}$$



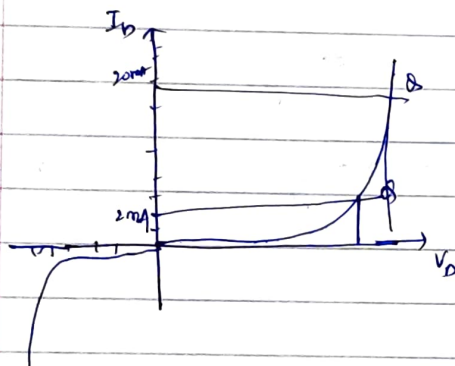
$$r_{avg} = \frac{\Delta V_D}{\Delta I_D} \quad \left| \begin{array}{l} \text{Pt - Pt} \end{array} \right.$$

8. Determine the DC resistance levels at (i) $I_D = 2 \text{ mA}$,
 (ii) $I_D = 20 \text{ mA}$,
 (iii) $V_D = -10 \text{ V}$.

a. For the characteristic curve:-

(a) Determine the AC resistance at $I_D = 2 \text{ mA}$

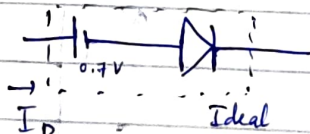
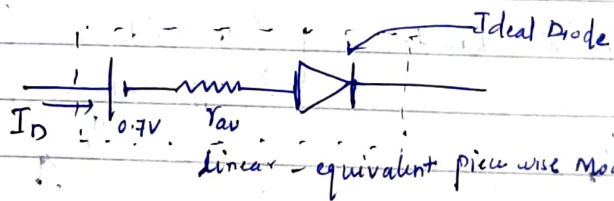
(b) Determine the AC resistance at $I_D = 20 \text{ mA}$

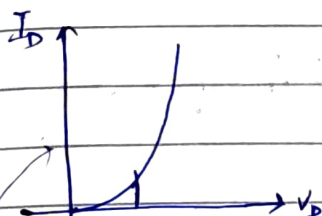


$$R_D (\text{at } I_D = 2 \text{ mA}) = \frac{V_{DB}}{2 \text{ mA}}$$

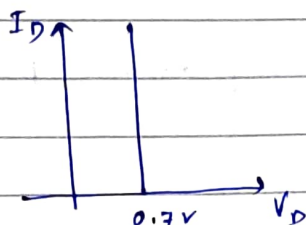
$$R_D (\text{at } I_D = 20 \text{ mA}) = \frac{V_{DB}}{20 \text{ mA}}$$

Diode equivalent circuit

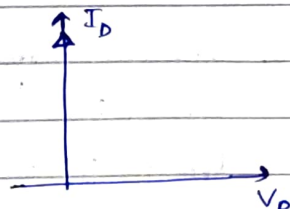




LE PWM



Ideal



Ideal diode

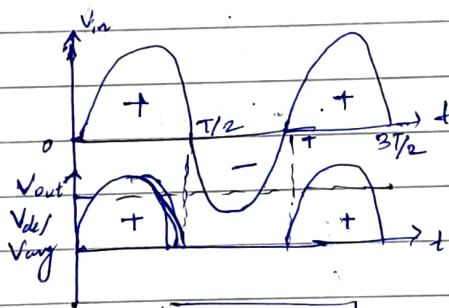
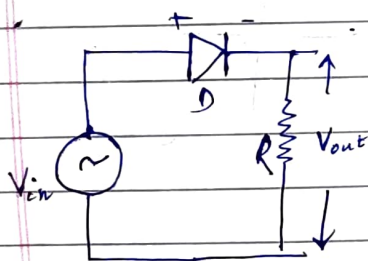
Rectifiers (A.C to D.C)

Half wave Rectifier

Full wave Rectifier

Center-tap

Bridge



Peak Inverse Voltage

$$P_{IV} = V_m$$

$$V_{av}/V_{dc} = \frac{1}{T} \int_0^{T/2} V_m \sin \omega t \, dt = 0.318 V_m = \frac{V_m}{\pi}$$

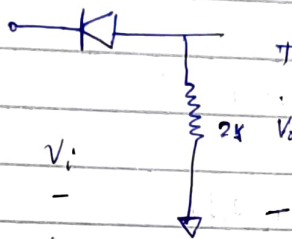
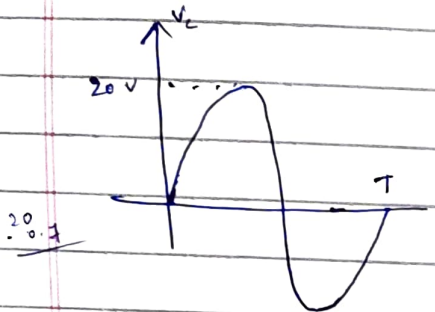
$$V_{rms} = \frac{1}{T} \int_0^{T/2} (V_m \sin \omega t)^2 \, dt = \frac{V_m}{\sqrt{2}}$$

If V_T , then $V_{dc} \approx 0.318 (V_m - V_T)$

Q. Sketch the output V_o and determine DC level of output for the network :-

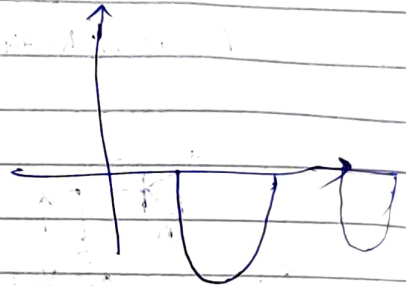
(i) Repeat if ideal diode is silicon diode

(ii) Repeat if V_m is 200V and compare the result to ans 1.



$$V_{dc} = 0.318 \times 20 \quad V_i = 0.7$$

$$\begin{aligned} V_{dc} &= 0.318 (20 - 0.7) \\ &= 0.318 \times 19.3 \\ &= 6.1374 \end{aligned}$$



$$\begin{aligned} V_{dc} &= 0.318 \times 200 \\ &= 63.6 \end{aligned}$$

Efficiency of HWR

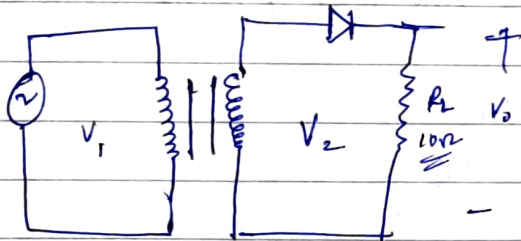
$$\eta = \frac{\text{d.c. o/p power}}{\text{A.c. I/P power}} = \frac{P_{dc}}{P_{ac}} = \frac{V_{dc} \cdot I_{dc}}{V_{ac} \cdot I_{ac}}$$

$$V_{dc} = \frac{V_m}{\pi} \quad I_{dc} = \left(\frac{V_m}{\pi} \right) / R_L \quad I_f(r_f) \cdot I_{dc} = \frac{V_m}{\pi} / (R_L + r_f)$$

$$P_{dc} = I_{dc} \times V_{dc} = \frac{V_m}{\pi} \cdot \frac{I_m}{\pi} = \left(\frac{I_m}{\pi} \right)^2 R_L$$

$$P_{ac} = I_{rms}^2$$

Q. A AC supply of 230 V is applied to a half Wave rectifier through a transformer ratio 10:1, Find the output DC power and peak inverse voltage of HWR.



$$V_{rms} = 230 \text{ V}$$

$$V_m = V_{rms} \times \sqrt{2}$$

$$= 230 \times \sqrt{2} = 325 \text{ V}$$

$$\frac{V_1}{V_2} = \frac{N_1}{N_2} = \frac{10}{1}$$

$$V_{dc} = \frac{V_m}{\pi} = \frac{325}{\pi}$$

$$\frac{325}{V_2} = \frac{10}{1}$$

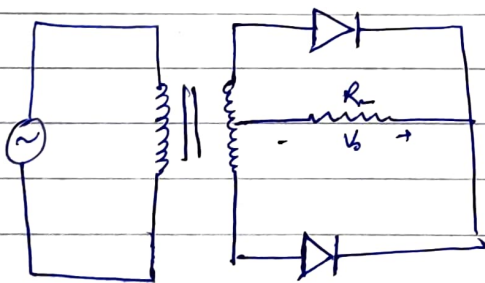
$$V_2 = 32.5$$

$$P_{dc} = \frac{(V_{dc})^2}{R_L} = \left(\frac{32.5}{\pi} \right)^2 \cdot \frac{1}{10}$$

$$P_{iv} = 32.5$$

Full wave Rectifier

Center-tap Rectifier



$$P_{iv} = 2 V_m$$

$$V_{rms} = \frac{V_m}{\sqrt{2}}$$

$$V_{dc} = \frac{1}{T} \int_0^T V_m \sin \omega t \, dt$$

$$V_{rms} = \frac{1}{T} \int_0^T (V_m \sin \omega t)^2 \, dt$$

If V_T then $V_{dc} = \frac{2(V_m - V_T)}{\pi}$

- Q. A FWR uses 2 diodes, the internal resistance of each diode is $20\ \Omega$. The transformer RMS secondary voltage from centre tap to each end of secondary is 50V and load resistance is $980\ \Omega$. Find the mean load current and the rms value of current.

$$V_m = V_{\text{rms}} \times \sqrt{2} = 50\sqrt{2}$$

$$I_m = \frac{V_m}{r_f + R_L} = \frac{50\sqrt{2}}{20 + 980} = \frac{50\sqrt{2}}{1000}$$

$$I_{dc} = \frac{2I_m}{\pi} = 45\text{ mA}$$

$$I_{\text{rms}} = \frac{I_m}{\sqrt{2}} = 50\text{ mA}$$

Efficiency calculation (η)

$$I_{dc} = \frac{2I_m}{\pi}$$

$$P_{dc} = I_{dc}^2 \times R_L = \left(\frac{2I_m}{\pi}\right)^2 R_L$$

$$P_{ac} = I_{\text{rms}}^2 (r_f + R_L)$$

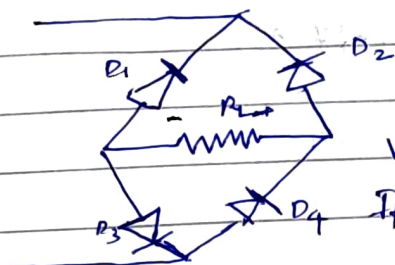
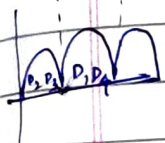
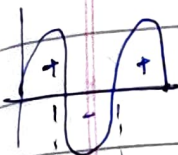
$$I_{\text{rms}} = I_m / \sqrt{2}$$

$$\eta = \frac{P_{dc}}{P_{ac}} = \frac{\left(\frac{2I_m}{\pi}\right)^2 R_L}{\left(\frac{I_m}{\sqrt{2}}\right)^2 (r_f + R_L)}$$

$$= \frac{0.812 R_L}{r_f + R_L} = 0.812 = 81.2\%$$

$$\text{F.W.R}(\eta) = 2 \times \text{H.W.R}(\eta)$$

Full Wave Bridge Rectifier:-



$$P_{IV} = V_m$$

$$V_{rms} = \frac{V_m}{\sqrt{2}}$$

$$V_{dc} = 2 [0.318 V_m] = 0.636 V_m$$

$$\text{If } V_T, \text{ then } V_{dc} = 0.636 (V_m - 2V_T)$$

Ripple factor:-

$$\text{Ripple factor} = \frac{I_{ac}}{I_{dc}}$$

$$I_{rms} = \sqrt{I_{dc}^2 + I_{ac}^2}$$

$$I_{ac} = \sqrt{I_{rms}^2 - I_{dc}^2}$$

$$= \frac{1}{I_{dc}} \sqrt{I_{rms}^2 - (I_{dc})^2}$$

$$\text{H.W.R} \rightarrow \text{Ripple factor} = \sqrt{\left(\frac{I_{rms}}{I_{dc}}\right)^2 - 1} = \sqrt{\left(\frac{I_m/2}{I_m/\pi}\right)^2 - 1} = 1.21$$

$$\text{F.W.R} = \sqrt{\quad}$$

Q. For a full wave bridge rectifier with 120V rms, sinusoidal input has a load resistor of 1kΩ

(a) If silicon diodes are employed what is the V_{dc} available at load.

(b) Determine the required PIV rating of each diode.

(c) Find the max^m current through each diode during conduction.

(d) What is the required power rating of each diode.

$$V_T = 0.7 \quad V_{rms} = 120V$$

$$V_{dc} = 0.636 (120\sqrt{2} - 1.4) = 106.59$$

$$= 0.636 (169.7 - 1.4) = 106.59$$

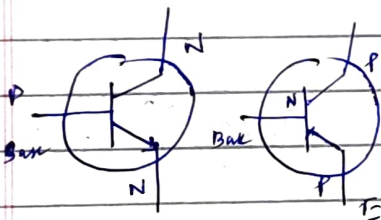
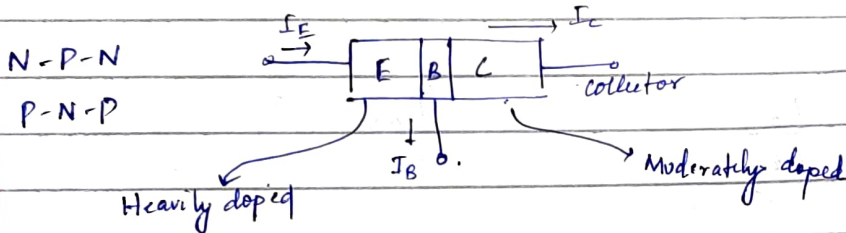
$$P_{iv} = V_m = 169.7$$

$$I_{dc} = \frac{V_{dc}}{R}$$

$$I_m = \frac{V_m}{R_L} = \frac{169.7}{1000} = 0.1697 \text{ A}$$

$$P_{ave} \text{ rating} = \frac{V_{ac}}{I_{dc}} = 106.59$$

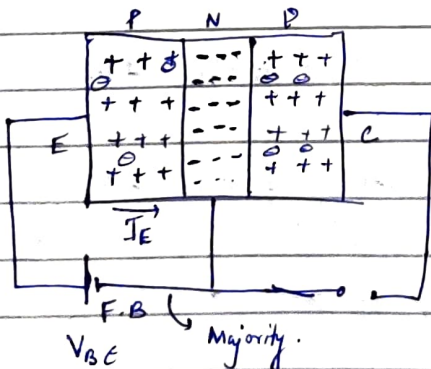
BJT (Bipolar Junction Transistor)

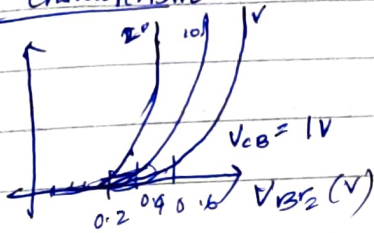


- common - base configuration
- common - emitter configuration
- common - collector configuration
- Active region
- Saturation region
- cutoff region

$\alpha \rightarrow$ amplification factor in C.B

$\beta \rightarrow$ amplification factor in

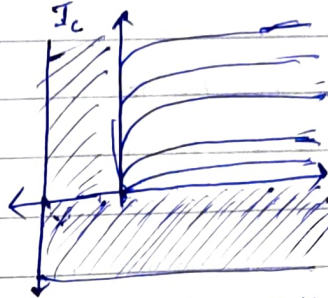


I/P characteristic

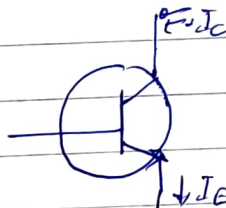
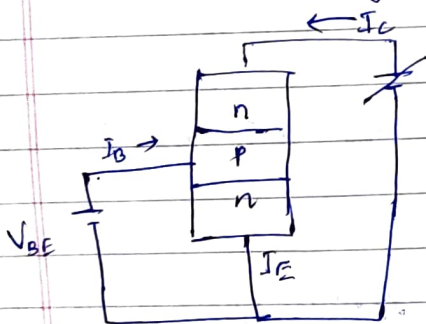
$$\alpha_{dc} = I_C / I_E$$

$$I_C = \alpha I_E + I_{CB}$$

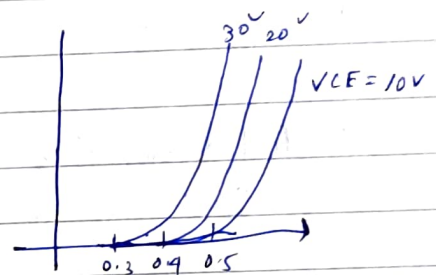
$$\alpha_{ac} = \frac{\Delta I_C}{\Delta I_E}$$

O/P characteristics

$$\alpha_o = \frac{\Delta V_{CE}}{\Delta I_C}$$

Common - Emitter Configuration:

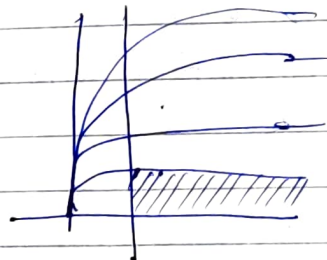
$$I_E = I_B + I_C$$



$$\beta_{dc} = \frac{I_C}{I_B}$$

$$I_C = \beta I_B$$

$$\beta_{ac} = \frac{\Delta I_C}{\Delta I_B}$$



$$I_C = \alpha I_E + I_{CB0}$$

$$= \alpha (I_C + I_B) + I_{CB0}$$

$$\alpha \approx 0.99$$

$$I_C = \frac{\alpha I_B}{1 - \alpha} + \frac{I_{CB0}}{1 - \alpha}$$

$$I_C \approx 250 I_{CB0}$$

$$\alpha \approx \frac{\beta}{1 + \beta} \quad \beta = \frac{\alpha}{1 - \alpha}$$

1. The saturation current density of P-n junction is 150 mA/m^2 at 300 K

Find the voltage that has to apply across a junction to cause a forward current density of 10^5 A/m^2 to flow.

2. Find the static and dynamic resistance of P-n junction Germanium diode if the temp. is 27°C and I_s is 1 micro A for the applied bias of 0.2 V .

3. Find the value of β if $\alpha = 0.9$, $\alpha = 0.98$, $\alpha = 0.99$

4. Calculate I in a transistor for which $\beta = 50$ and $I_B = 20 \text{ mA}$.

5. Find α rating of a transistor and determine the value of I_C using both α and β
 $I_B = 240 \text{ mA}$, $\beta = 49$

6. Collector leakage current of a transistor is 300 mA in C arrangement. If the transistor is connected in CB ~~transisto~~ arrangement. What will be the
Given

7. In CB connection emitter current is 1 milli A if emitter circuit is open
Collector



2.

R_D

$$I_S = 10$$

$$I_D = I_S \left(e^{\frac{V_D}{n V_T}} - 1 \right)$$

$$= 10^{-6} \left(e^{\frac{0.2}{1 \times 0.0258}} - 1 \right)$$

$$= 10^{-6} \left(e^{7.75} - 1 \right)$$

$$= 10^{-6} (2321.5 - 1)$$

$$= 2320.5 \times 10^{-6}$$

$$= \cancel{0.00232} \text{ A} \cdot 2.32 \text{ mA} \times 10^{-3} \text{ A}$$

$$R_D = \frac{V_D}{I_D} = \frac{0.2}{2.32 \times 10^{-3}} = 0.0862 \times 10^3 = 86.2 \Omega$$

$$R_{ac} = \frac{26 \text{ mV}}{I_D} = \frac{26 \times 10^{-3}}{2.32 \times 10^{-3}} = 1.07 \text{ mA}$$

3.

$$\alpha = 0.9$$

$$\beta = \frac{\alpha}{1 - \alpha} = \frac{0.9}{1 - 0.9} = \frac{0.9}{0.1} = 9$$

$$\alpha = 0.98$$

$$\beta = \frac{\alpha}{1 - \alpha} = \frac{0.98}{1 - 0.98} = \frac{0.98}{0.02} = 49$$

$$\alpha = 0.99$$

$$\beta = \frac{\alpha}{1 - \alpha} = \frac{0.99}{1 - 0.99} = \frac{0.99}{0.01} = 99$$

4.

$$I_E = 1.02 \text{ mA}$$

$$V_T = \frac{kT}{q}$$

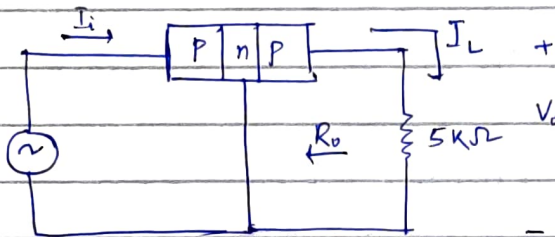
$$= \frac{1.38 \times 10^{-23} \times 300}{1.6 \times 10^{-19}}$$

$$= \frac{1.38 \times 300}{1.6} \times 10^{-4}$$

$$= 258.75 \times 10^{-4}$$

$$= 0.0258$$

Transistor As an amplifier

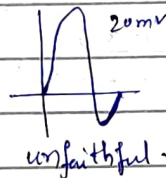
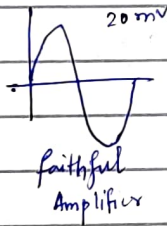
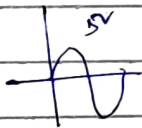
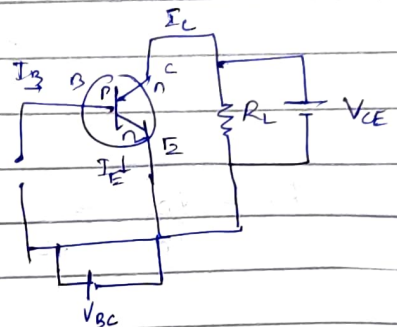
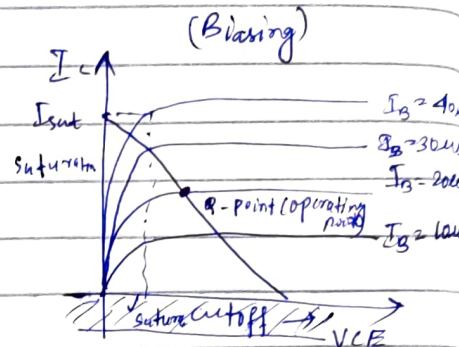


$$I_i = \frac{V_i}{R_i} = \frac{200 \text{ mV}}{20 \Omega} = 10 \text{ mA}$$

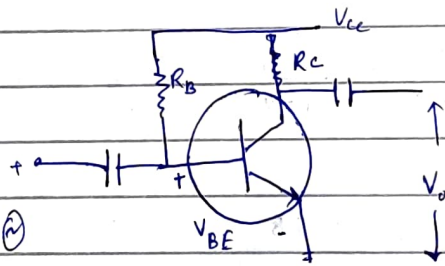
$$I_L = I_i = 10 \text{ mA}$$

$$I_L = I_C = 10 \text{ mA}$$

$$V_o = I_L \cdot R = (10 \text{ mA}) (5 \text{ k}\Omega) = 50 \text{ V}$$



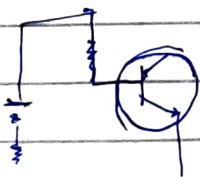
- ① Fixed bias configuration
- ② Emitter bias configuration
- ③ Voltage divider bias
- ④ Voltage - Feedback bias.



D-C Analysis of Transistor

Remove all A.C and capacitor open.

I/P Loop



$$V_{CE} = 0, I_{C \text{ sat}} = \frac{V_{CC}}{R_C}$$

$$I_C = 0, V_{CE \text{ sat}} = V_{CC}$$

For the fixed bias configuration determine I_{CQ} , I_{BQ} , V_{CEQ} , V_C , V_B , V_E .

$$R_B = 470\text{K}, R_C = 2.7\text{K}, V_{CC} = 16\text{V}.$$

$$\begin{array}{r} 16 \\ - 0.7 \\ \hline 15.3 \end{array}$$

$$V_{CC} - I_B R_B - V_{BE} = 0$$

$$16 - I_B (470\text{K}) - 0.7 = 0$$

$$16 - 0.7 = I_B \times 470 \times 10^3$$

$$I_{BQ} = \frac{15.3}{470} \times 10^{-3} = 0.0325 \times 10^{-3}$$

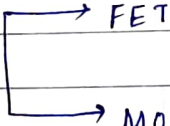
$$= 32.55 \times 10^{-6} \text{ A}$$

$$= \underline{\underline{32.55 \mu\text{A}}}$$

$$I_{CQ} = \beta \cdot I_{BQ} = 100 \times 32.55 \mu\text{A} = 3.25 \text{ mA}.$$

FET (Field effect Transistor)

JFET

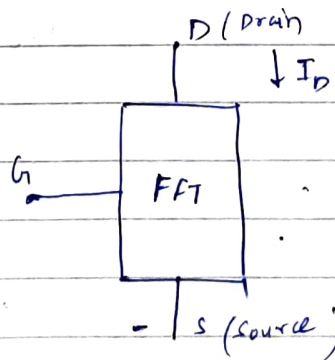
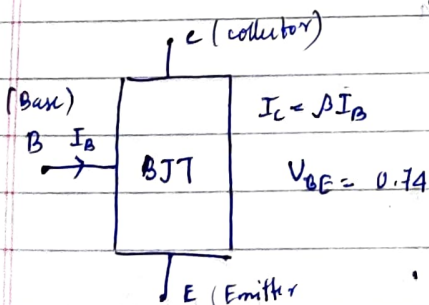


MOSFET

Depletion type MOSFET $\rightarrow$ D-MOS

Enhancement type MOSFET $\rightarrow$ E-MOS

- BJT vs FET
- Construction operation
- MOSFET (N type & P-type)
- D-MOS (N type & P-type)
- E-MOS (N type & P-type)



BJT

(i) It is a Bipolar device that is current conduction due to two types of carriers e^- & holes

(ii) Input of BJT is forward bias having low input Impedance.

(iii) BJT is a current control device and ~~FET is a voltage control device~~

(iv) In BJT two junctions

(v) Noise level is more in BJT

FET

(i) It is a unipolar device i.e. due to current conduction due to one type of carrier.

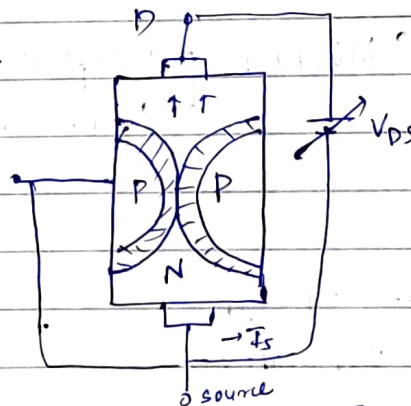
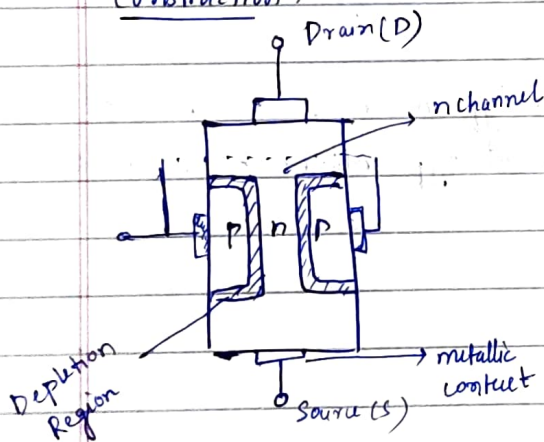
(ii) Input of FET is reverse bias hence.

(iii) FET is a voltage control device.

(iv) In FET no junctions

(v) Noise level is low in BJT.

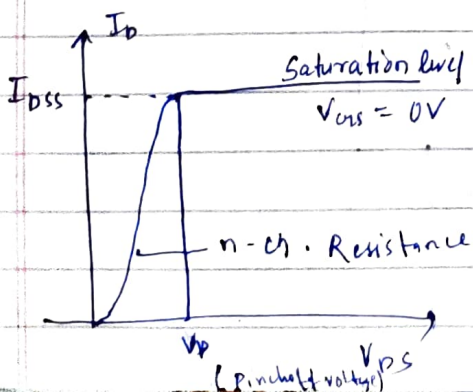
Construction:



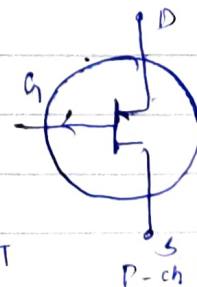
I_{DSS}
↓ shorted gate drain current

$$I_D = I_{DSS} \left(1 - \frac{V_{GS}}{V_P} \right)^2$$

Schokley's eqⁿ.



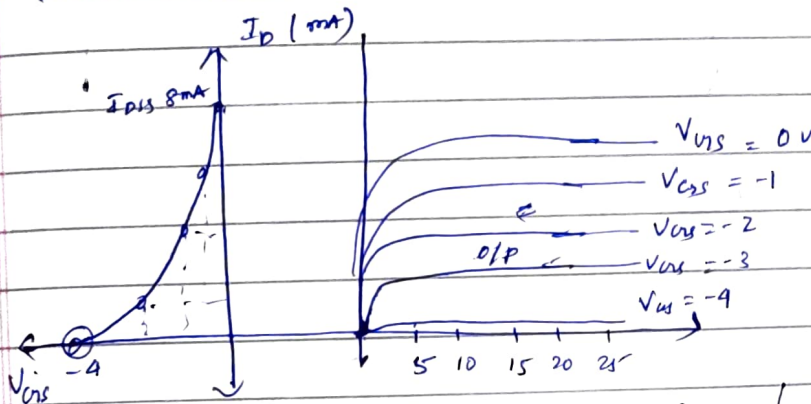
N-channel FET



P-channel FET



Transfer characteristics



V_{DS}	V_P
0	I_{DSS}
$0.3 V_P$	$I_{DSS} / 2$
$0.5 V_P$	$I_{DSS} / 4$
V_P	0 mA

$$I_D = I_{DSS} \left(1 - \frac{V_{GS}}{V_P}\right)^2$$

$$V_{GS} = 0, I_D = I_{DSS}$$

$$V_{GS} = V_P, I_D = 0 \text{ mA}$$

$$I_D = I_{DSS} \left(1 - \frac{V_{GS}}{V_P}\right)^2$$

$$\left(1 - \frac{V_{GS}}{V_P}\right)^2 = \frac{I_D}{I_{DSS}}$$

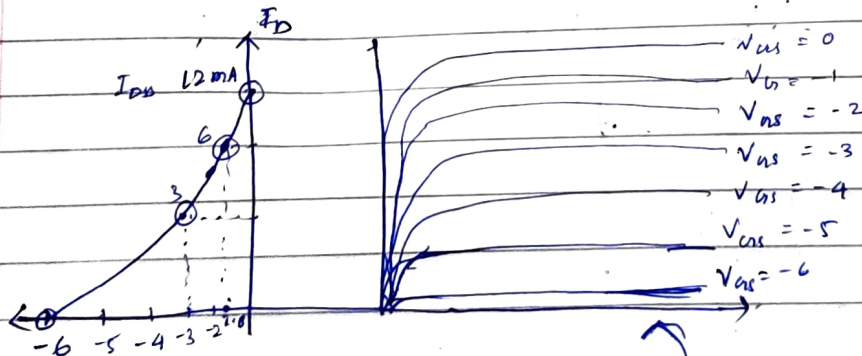
$$1 - \frac{V_{GS}}{V_P} = \sqrt{\frac{I_D}{I_{DSS}}}$$

$$V_{GS} = V_P \left(1 - \sqrt{I_D / I_{DSS}}\right)$$

Q7. Draw the transfer characteristics.

$$I_{DSS} = 8 \text{ mA}, V_P = -4 \text{ V}$$

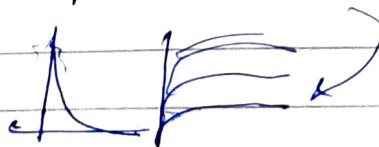
Q8. Sketch the transfer characteristics defined by $I_{DSS} = 12 \text{ mA}$ and $V_P = -6 \text{ V}$



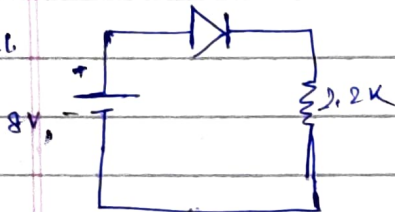
V_{GS}	V_P
0	I_{DSS}
-1.8	$I_{DSS} / 4$
-3.0	$I_{DSS} / 9$
-6	0

positive $V_P \rightarrow$ N-ch

$-V_P \rightarrow$ P-channel



Q.1



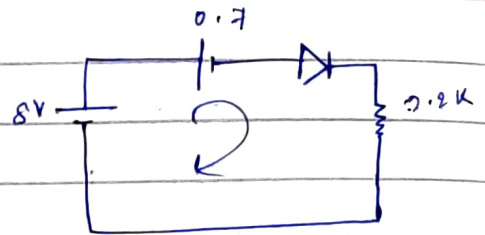
$$V_D = ?$$

$$V_R = ?$$

$$I_D = ?$$

$$V_D = 8 - 0.7$$

$$= 7.3$$

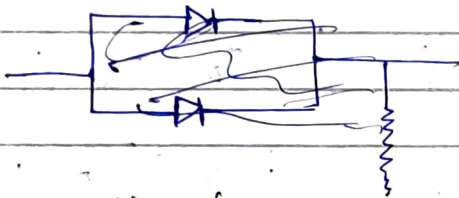


$$8 - 0.7 - 2.2 I_D = 0$$

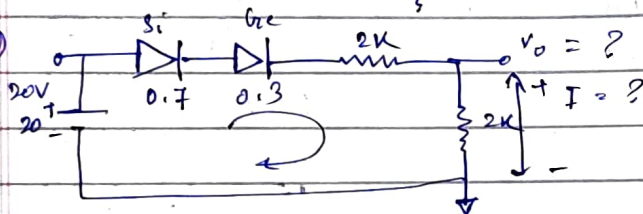
$$7.3 = 2.2 I_D$$

$$\Rightarrow I_D = \frac{7.3}{2.2} = \underline{\underline{3.31 \text{ mA}}}$$

Q.2



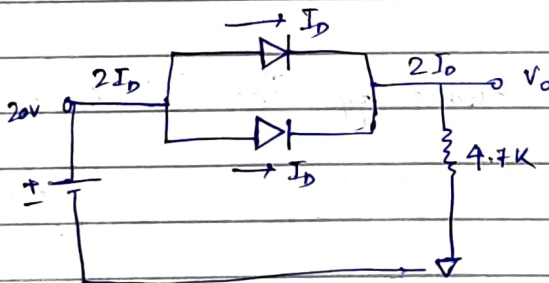
Q.2



$$20 - 0.7 - 0.3 - 4 I = 0$$

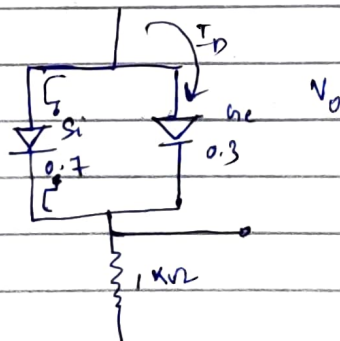
$$\Rightarrow I = \left(\frac{19}{4} \right) \text{ mA}$$

Q.3



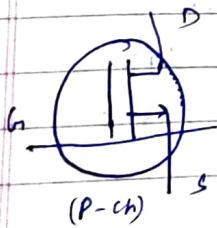
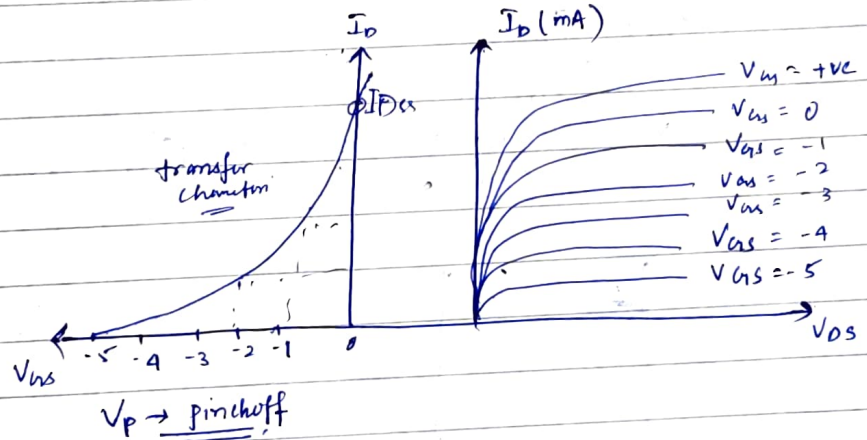
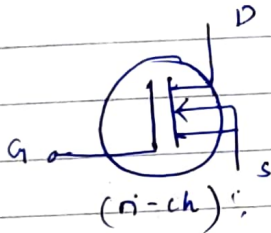
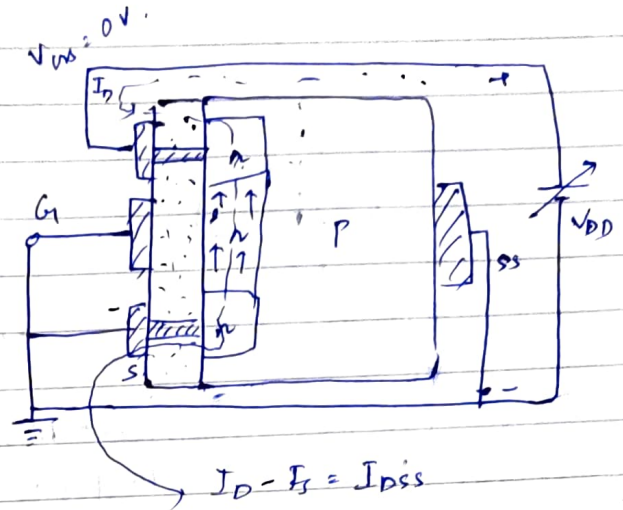
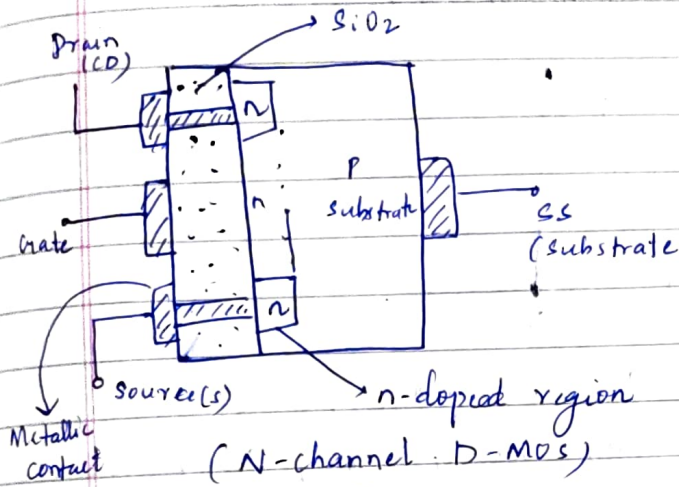
$$20 - 0.7 - 2 \times 4.7 \text{K} \times I_D = 0$$

Q.4

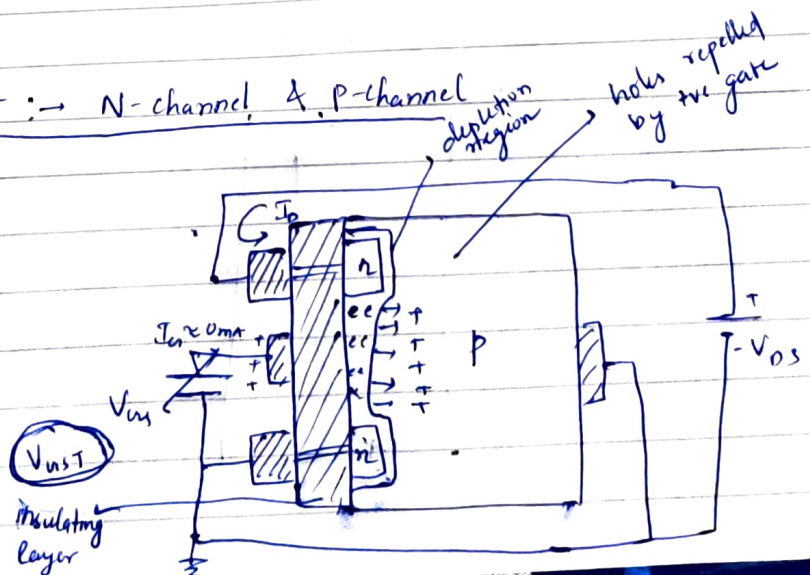
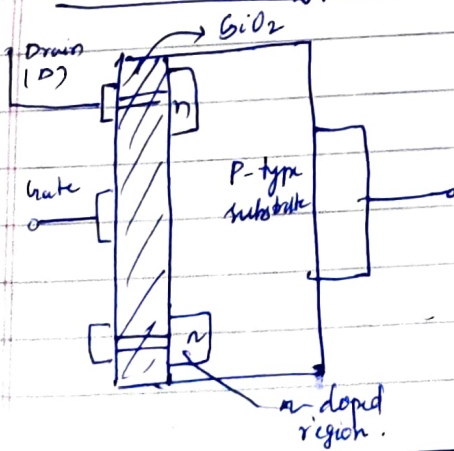


$$10 - 0.3$$

Depletion type of MOSFET (D-MOS)

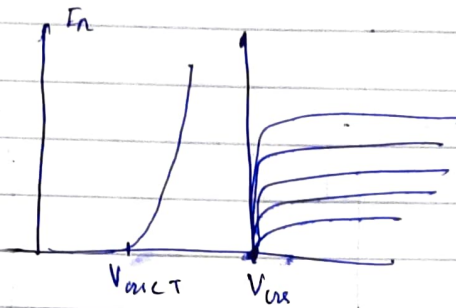
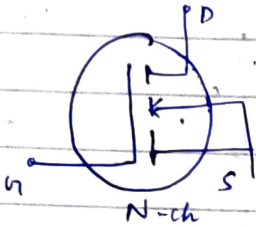


Enhancement type MOSFET :→ N-channel & P-channel



$$I_D = K (V_{GS} - V_T)^2$$

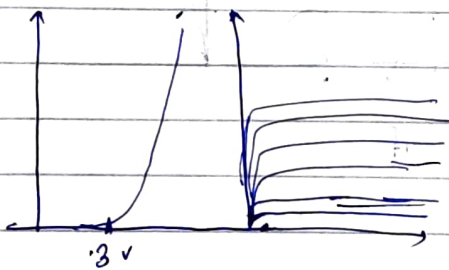
$$K = \frac{I_{D(on)}}{(V_{GS(on)} - V_T)^2}$$



Q: For the enhancement MOSFET $I_{D(on)} = 3 \text{ mA}$, $V_{GS(on)} = 10 \text{ V}$ and $V_{th} = 3 \text{ V}$. Find out the resulting value of K and transfer characteristic.

$$K = \frac{I_{D(on)}}{(V_{GS(on)} - V_T)^2} = \frac{3 \times 10^{-3}}{7^2}$$

$$K = \frac{3 \text{ mA}}{(10 - 3)^2} = 0.061 \times 10^{-3} \text{ A/V}^2$$



$$I_D = 0.061 \times 10^{-3} (15 - 3)^2$$

$$= 0.732 \times 10^{-3}$$

$$V_{GS} = 11 \text{ V}$$

$$I_D = 0.061 \times 10^{-3} (11 - 3)^2$$

$$= 0.061 \times 10^{-3} (8)^2$$

$$= 0.488 \times 10^{-3}$$

$$I_D = 0.061 \times 10^{-3} (12 - 3)^2$$

$$= 0.549 \times 10^{-3}$$

