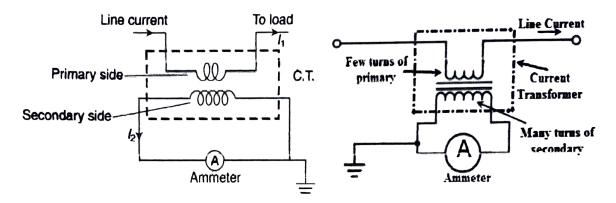
# MODULE IV

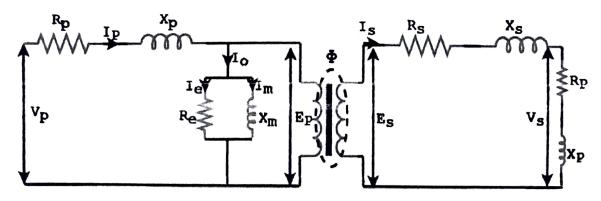
#### **CURRENT TRANSFORMERS (CT):-**

- The primary winding of a current transformer is connected in series with the fine carrying the main current.
- The secondary winding of the CT, where the current is many times stepped down, is directly connected across an ammeter, for measurement of current; or across the current coil of a wattmeter, for measurement of power; or across the current coil of a watt-hour meter for measurement of energy; or across a relay coil.
- The primary winding of a CT has only few turns, such that there is no appreciable voltage drop across it, and the main circuit is not disturbed.
- The current flowing through the primary coil of a CT, i.e., the main circuit current is primarily determined by the load connected to the main circuit and not by the load
- One of the terminals of the CT is normally earthed to prevent any accidental damage to the operating personnel in the event of any incumbent insulation breakdown.



When a typical name plate rating of a CT shows 500/5 A 10VA 5P20, it indicates that the CT rated primary and secondary currents are 500 A and 5 A respectively, its rated secondary burden is 5 VA, it is designed to have 5% accuracy and it can carry up to 20 times higher current than its rated value while connected in line to detect fault conditions, etc. urden) connected to the CT secondary.

## Equivalent Circuit of Current Transformer(CT) :-



The CT primary has few turns, and it has very little resistance. Rp and Xp, respectively, denote the primary winding resistance and reactance. The secondary winding resistance and reactance are denoted by R<sub>a</sub> and X<sub>a</sub> respectively. The magnetization components of the current transformer are Rc and  $X_m$ .  $R_c$  is responsible for the core loss component, and  $X_m$  is the magnetization reactance of CT.

Where,

n = Turn ratio

r, = Secondary winding resistance

 $X_s = Secondary winding reactance$ 

Rurdon connected to CT secondary

 $X_{\bullet} = Burden reactance connected to CT secondary$ 

 $E_p = Induced EMF in CT primary$ 

E, = Induced EMF in CT secondary

 $N_p = Primary turns of CT$ 

M, - Secondary turns of CT

 $I_p = CT$  primary current

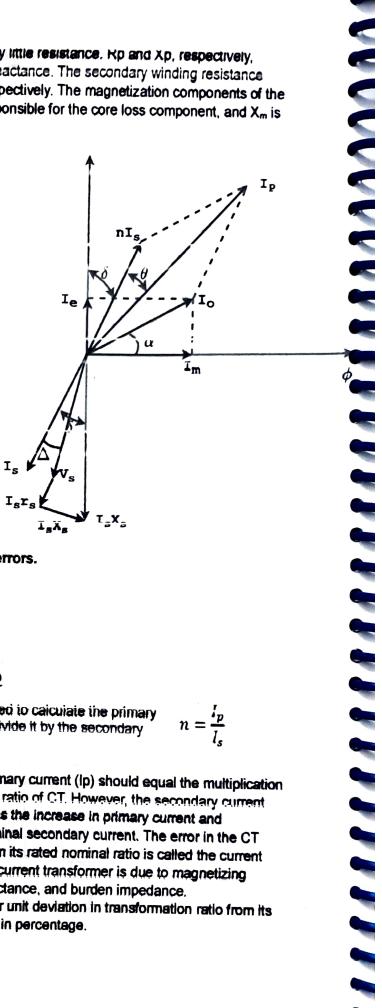
 $I_s = CT$  secondary current

I<sub>m</sub> = CT Magnetizing current

 $I_o = CT$  excitation current

\$ = Flux in CT core

 $\theta = Phase angle of CT$ 



The current transformer has two types of errors.

- Ratio Error
- Phase Angle Error

# **CT Transformation Ratio**

To find the transformation ratio, we need to calculate the primary current lp, as per the definition, and divide it by the secondary current is

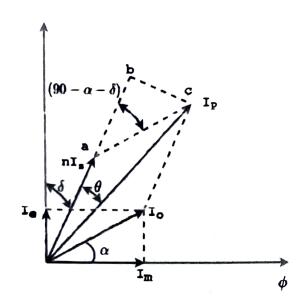
$$n = \frac{I_p}{I_s}$$

#### Ratio Error of Current Transformer

In an ideal current transformer, the primary current (Ip) should equal the multiplication of the secondary current and the turns ratio of CT. However, the secondary current does not vary in the same proportion as the increase in primary current and secondary current is less than the nominal secondary current. The error in the CT due to the difference in the current from its rated nominal ratio is called the current error or ratio error. The ratio error in a current transformer is due to magnetizing current, core loss current, leakage reactance, and burden impedance,

The CT ratio Error is defined as the per unit deviation in transformation ratio from its nominal ratio. Ratio error is expressed in percentage.

$$= \frac{Nominal\ ratio\ - Transformation\ ratio}{Transformation\ ratio}\ X\ 100$$



From the above phasor, the primary current lp is the phasor sum of nl<sub>a</sub> and l<sub>0</sub>. The CT primary current lp can be calculated using the vector addition formula.

$$\begin{split} I_p &= \sqrt{I_0^2 + (nI_s)^2 + 2 \, I_o \, nI_s \, Cos(90 - \alpha - \delta)} \\ I_p &= \sqrt{I_0^2 + (nI_s)^2 + 2 \, I_o \, nI_s \, Sin(\alpha + \delta)} \\ The \, CT \, Ratio \, is \, equal \, to \, ratio \, of \, I_p \, / \, Is \\ R &= \frac{I_p}{I_s} \\ R &= \frac{\sqrt{I_0^2 + (nI_s)^2 + 2 \, I_o \, nI_s \, Sin(\alpha + \delta)}}{I_s} \end{split}$$

The magnetizing current lo is very small compared to the primary current  $l_p$ . Therefore, the above expression can be simplified as follows.

$$R = \frac{\sqrt{I_0^2 + (nI_s)^2 + 2 I_o nI_s Sin(\alpha + \delta)}}{I_s}$$

$$R = \frac{\sqrt{[(nI_s)^2 + (I_0 Sin(\alpha + \delta))^2 + (2 I_o nI_s Sin(\alpha + \delta))]}}{I_s}$$

$$R = \frac{\sqrt{[nI_s + (I_0 Sin(\alpha + \delta))]^2}}{I_s}$$

$$R = \frac{nI_s + I_0 Sin(\alpha + \delta)}{I_s}$$

$$R = n + \frac{I_o Sin(\alpha + \delta)}{I_s}$$

$$R = n + \frac{I_o Sin(\alpha + \delta)}{I_s}$$

From the above expression, it is clear that the transformation ratio is not equal to the turn ratio. The transformation ratio and turn ratio will be equal if  $\alpha$ =0 and  $\delta$ =0. This condition can be achieved if the core loss is equal to zero and the burden is purely resistive. This is an ideal condition. However, this condition is practically impossible.

#### #Ratio Error of Current Transformer for Resistive Burden

Since the burden of the CT is generally resistive. Therefore, the power factor of the burden is unity, and hence  $\delta$ =0

$$R = n + \frac{I_o Sin(\alpha + \delta)}{I_s}$$

$$\delta = 0 \text{ for resitive burden}$$

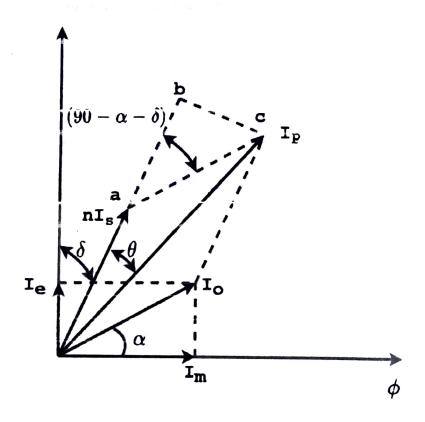
$$R = n + \frac{I_o Sin\alpha}{I_s}$$

$$R = n + \frac{I_e}{I_s} \quad Since \left[I_o Sin\alpha = I_o\right]$$

## Phase Angle Error of the Current Transformer:-

The primary and secondary current of the CT should be out of phase, meaning the phase angle between the primary and secondary must be 180 degrees. Any deviation in the phase angle from 180 degrees is called the phase angle error of the CT.

The phase angle of the current transformer is defined as the angle between the primary current ip and secondary current  $l_s$ . In the above phasor diagram,  $\theta$  is the phase angle.



Consider the right angle triangle ABC in the above phasor diagram.

$$tan\theta = \frac{bc}{ob}$$

$$= \frac{I_0 Sin(90 - \alpha - \delta)}{oa + ab}$$

$$= \frac{I_0 Cos(\alpha + \delta)}{[nI_s + I_0 Sin(\alpha + \delta)]}$$

Since  $\theta$  is very small, so  $\tan \theta = \theta$ 

$$\theta = \frac{l_0 Cos(\alpha + \delta)}{[nl_2 + l_0 Sin(\alpha + \delta)]}$$

Also  $I_0$  is very small and,  $I_0$  Sin $(\alpha + \delta) \ll \ll nI_s$ 

hence  $l_0 Sin(\alpha + \delta)$  can be neglected

$$\theta = \frac{I_0 Cos(\alpha + \delta)}{nI_s}$$

$$\theta = \frac{I_0 (Cos\alpha Cos\delta - Sin\alpha Sin\delta)}{nI_s}$$

$$\theta = \frac{I_0 Cos\alpha Cos\delta - I_0 Sin\alpha Sin\delta}{nI_s}$$

From Phasor,  $I_0 Cosa = I_m$  and  $I_0 Sina = I_e$ 

$$\theta = \frac{I_m \cos \delta - I_e \sin \delta}{nI_s} Radians$$

$$\theta = 180/\pi \frac{(I_m \cos \delta - I_e \sin \delta)}{nI_e}$$
 Degree

# Phase Angle Error of Current Transformer For Resistive Burden

The phase angle between the primary and secondary of the current transformer must be 180 degrees. The primary and secondary current must be out of phase. The phase angle error is the deviation in the phase angle of the primary and secondary current. The phase angle between the primary and secondary current of the CT is denoted by angle  $\theta$ .

Since the CT burden is generally resistive, the <u>power factor</u> of the burden is unity, and hence  $\delta$ =0. The following expression gives the phase angle error of CT.

$$\theta = 180/\pi \frac{(I_m \cos \delta - I_e \sin \delta)}{nI_s}$$

$$\theta = 180/\pi \frac{(I_m \cos 0 - I_e \sin 0)}{nI_s}$$

$$\theta = (\frac{180}{\pi}) \frac{I_m}{nI_s} \text{ Degree}$$

## Causes of Errors in CT:-

In an ideal CT, the actual transformation ratio should have been exactly equal to the turns ratio andthe phase angle should have been zero. However, due to inherent physical limitations to the electric and magnetic circuits of the CT, practical performance deviates from these ideal behaviors and errors are introduced in measurement. The reasons for these emors are given here.

- Primary winding always needs some magnetising MMF to produce flux and, therefore, the CT draws the magnetising current IM.
- CT no-load current must have a component lc that has to supply the core losses, i.e., the eddy current loss and the hysteresis loss.
- Once the CT core becomes saturated, the flux density in the core no longer remains a linear function of the magnetising force, this may introduce further errors.
- Primary and secondary flux linkages differ due to unavoidable flux leakages.

# Reducing Errors in CT:-

Errors are produced in the ratio and phase angle of a CT owing to the presence of the noload component of the primary current. Improvement of accuracy, then, depends upon minimizing this component or nullifying in some way its effects in introducing errors. The most obvious idea would be to attempt to keep the magnetizing current component as small as possible. This can be achieved by a combination of the following schemes:

#### Low Flux Density

The magnetising component of current may be restricted by using low values of flux density. This may be achieved by using large cross-section for core. For this reason, CTs are normally designed with much lower flux densities as compared to a normal power transformer.

- High Permeability Core Material
  - The magnetising component of current may be made small by the use of high permeability core material. 50% Fe + 50% Ni has high permeability at low flux densities along with reasonably high saturation density value. It is used frequently as core material for manufacturing CTs.
- **Modification of Turns Ratio** 
  - The accuracy of current transformers may be improved, at least in terms of transformation ratio, by suitably modifying the actual number of turns.
- If the secondary current is found to be too high, it may be reduced by a shunt placed across the primary or secondary. Use of shunts can also help in reducing the phase-angle error.
- **Wound-Core Construction**
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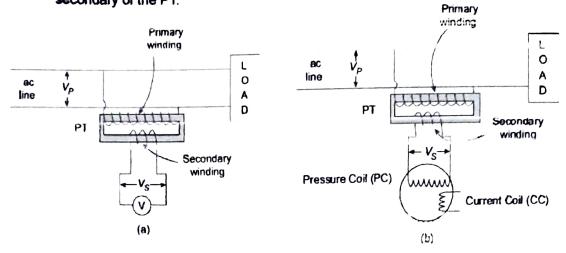
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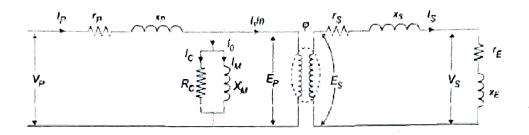
  lay be achieved
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  y be utilised in An improvement in the magnetisation characteristics of the CT core may be achieved by the use of wound-core construction. This type of construction for the core has been in use for some time in distribution transformers. By special treatment of the silicon steel to be used as core material, and by using it to carry flux always in the direction of grain orientation (rolling the sheet steel in proper way), magnetic properties of the core can be largely improved. This improvement may be utilised in CTs to reduce the ratio and phase angle errors.

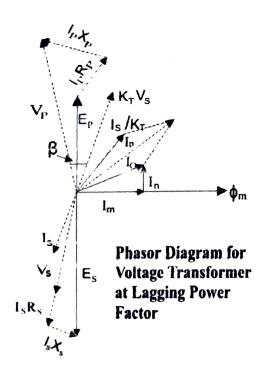
# POTENTIAL TRANSFORMERS (PT):-

The primary winding of the PT is connected across the high-voltage line whose voltage is to be measured and the measuring instruments are connected across the secondary of the PT.



#### Equivalent circuit:-





Is - Secondary current.

E<sub>s</sub> - Secondary induced emf.

V<sub>s</sub> - Secondary terminal voltage.

R<sub>s</sub> - Secondary winding resistance.

X<sub>s</sub> - Secondary winding reactance.

I<sub>p</sub> - Primary current.

E<sub>p</sub> - Primary induced emf.

V<sub>o</sub> – Primary terminal voltage.

Rp - Primary winding resistance.

X<sub>p</sub> - Primary winding reactance.

K<sub>T</sub> - Turns ratio = Numbers of primary turns/number of secondary turns.

lo - Excitation current.

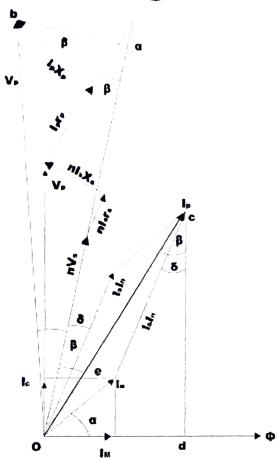
Im - Magnetizing component of Io.

lw - Core loss component of lo.

 $\Phi_m$  – Main flux.

 $\beta$  – Phase angle error.

# **Expanded view of Phasor Diagram**



The phase angle between the primary voltage and the secondary voltage is called the phase angle of PT. This phase angle is ideally equal to zero because these two phasors are in same phase.

From the phasor diagram we have,

$$\begin{split} V_p &= E_p + I_p R_p + I_p X_p = n E_s + I_p R_p + I_p X_p \\ V_p &= n (V_s + I_s R_s + I_s X_s) + I_p R_p + I_p X_p = n V_s + n I_s R_s + n I_s X_s + I_p R_p + I_p X_p \\ O_a &= V_p \cos \Theta \\ O_a &= n V_s + n I_s R_s \cos \delta + n I_s X_s \sin \delta + I_p R_p \cos \beta + I_p X_p \sin \Theta \\ V_p \cos \Theta &= n V_s + n I_s R_s \cos \delta + n I_s X_s \sin \delta + I_p R_p \cos \beta + I_p X_p \sin \beta \\ V_p \cos \Theta &= n V_s + n I_s (R_s \cos \delta + X_s \sin \delta) + I_p R_p \cos \beta + I_p X_p \sin \beta \end{split}$$

But in reality, the phase angle is very small and the primary and secondary voltage are perpendicular to the flux and then;

$$<$$
ocd =  $\beta$  and  $<$ ecd =  $\delta$ 

Then

$$l_p \cos \beta = l_c + \frac{l_p}{n} \cos \delta \text{ and } l_p \sin \beta = l_M + \frac{l_p}{n} \sin \delta$$
 (2)

Hence  $V_D \cos \Theta = V_D$ 

Then.

Substituting the above value from eq 1 we get

$$V_{p} = nV_{s} + nI_{s}(R_{s}\cos\delta + X_{s}\sin\delta) + (I_{c} + \frac{I_{s}}{n}\cos\delta)R_{p} + \left(I_{m} + \frac{I_{s}}{n}\sin\delta\right)X_{p}$$

Or

$$V_p = nV_s + I_s \cos \delta \left( nr_s + \frac{\kappa_p}{n} \right) + I_s \sin \delta \left( nX_s + \frac{x_p}{n} \right) + (I_c R_p + I_m X_p)$$
 (3)

Or

$$V_p = nV_s + \frac{I_s}{n} (R_p \cos \delta + X_p \sin \delta) + (I_c R_p + I_m X_p)$$
(4)

Where K₃ is equivalent resistance of P1 and X₃ equivalent reactance of P1.

# **Phase Angle of Potential Transformer (PT)**

From the phasor diagram the terms Ip and Is are less compared to large voltage and these terms are neglected thus we get:

$$\tan \theta = \frac{l_p X_p \cos \beta - l_p R_p \sin \beta + n l_s X_s \cos \delta - n l_s R_s \sin \delta}{n V_s}$$

$$\tan \theta = \frac{X_\nu \left( I_c + \frac{l_s}{n} \cos \delta \right) - R_\nu \left( I_m + \frac{l_s}{n} \sin \delta \right) + n I_s X_s \cos \delta}{n V_s}$$

$$\tan \theta = \frac{l_s \cos \delta \left( \frac{X_p}{n} + n X_s \right) - l_s \sin \delta \left( \frac{R_p}{n} + n R_s \right) + l_c X_p - l_m R_p}{n V_s}$$

$$\tan \theta = \frac{\left( \frac{l_s \cos \delta}{n} \left( X_p + n^2 X_s \right) - \frac{l_s \sin \delta}{n} \left( R_p + n^2 R_s \right) + l_c X_p - l_m R_p}{n V_s}$$

$$\tan \theta = \frac{\frac{l_s \cos \delta}{n} X_p - \frac{l_s \sin \delta}{n} R_p + l_c X_p - l_m R_p}{n V_s}$$

$$\tan \theta = \frac{\frac{l_s \cos \delta}{n} \left( X_p \cos \delta - R_p \sin \delta \right) + l_c X_p - l_m R_p}{n V_s}$$

Let tan o = o, then

$$\theta = \frac{\frac{l_s}{n}(n^2X_s\cos\delta - R_p\sin\delta) + l_cX_p - l_mR_p}{nV_s}$$

$$\theta = \frac{\frac{l_s}{n}(n^2X_s\cos\delta - n^2R_s\sin\delta) + l_cX_p - l_mR_p}{nV_s}$$

$$\theta = \frac{nI_s(X_s\cos\delta - R_s\sin\delta) + l_cX_p - l_mR_p}{nV_s}$$

$$\theta = \frac{nI_s(X_s\cos\delta - R_s\sin\delta) + l_cX_p - l_mR_p}{nV_s}$$

So, the phase angle  $\Theta$  is:

$$\theta = \frac{l_s}{v_s} \left( X_s \cos \delta - R_s \sin \delta \right) + \frac{l_c X_p - l_m R_p}{n V_c}$$
 (7)

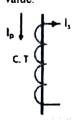
#### Basis for Comparison

#### **Current Transformer**

Definition

Transform the current from high value to the low

Circuit Symbol



Usually built up with lamination of silicon steel. Core

It carries the current which is to be measured **Primary Winding** 

Secondary Winding It is connected to the current winding of the

instrument.

Connected in series with the instrument Connection

Has a small number of turns Primary Circuit

Has a large number of turns and cannot be open Secondary Circuit

circuit.

5A or 1A Range High Transformation

Ratio Does not depends on secondary burden Burden

Constant current Input

The primary winding consists the full line current. Full line current

Two types ( Wound and Closed Core ) Types

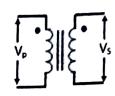
Low Impedance

Measuring current and power, monitoring the power **Applications** 

grid operation, for operating protective relay,

#### Potential Transformer

Transform the voltage from high value to the low value.



(6)

(7)

sformer

Itage from high value to

Vs

ith high quality steel that densities ge which is to be the meter or instrument.

Itlel with the instrument er of turns and can be condary burden the condary burden the condary burden that conditions are consists the full line comagnetic and Capacitor over source, operating It is made up of with high quality steel operating at low flux densities It carries the voltage which is to be measured.

It is connected to the meter or instrument.

Connected in parallel with the instrument.

Has a large number of turns

Has a small number of turns and can be open circuit.

110v Low

#### Depends on the secondary burden

Constant Voltage

The primary winding consists the full line voltage.

Two types (Electromagnetic and Capacitor

voltage) High

Measurement, power source, operating protective relay.

# MODULE IV

### **POTENTIOMETER**

A potentiometer is an instrument which is used for measurement of potential difference across a known resistance or between two terminals of a circuit or network of known characteristics.

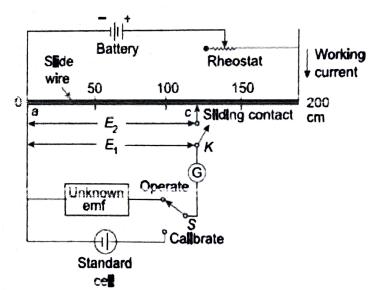
Some important characteristics of a potentiometer are the following:

- A potentiometer measures the unknown voltage by comparing it with a known voltage source rather than by the actual deflection of the pointer. This ensures a high degree of accuracy.
- 2) As a potentiometer measures using null or balance condition, hence no power is required for the measurement.
- Determination of voltage using a potentiometer is quite independent of the source resistance.
  - Since a potentiometer measures voltage by comparing it with a standard cell, it can be also used to measure the current simply by measuring the voltage drop produced by the unknown current passing through a known standard resistance.
  - By the potentiometer, power can also be calculated and if the time is also measured, energy can be determined by simply multiplying the power and time of measurement. Thus potentiometer is one of the most fundamental instruments of electrical measurement.

# DC potentiometer:-

#### Operation:-

 First, the switch S is put in the 'operate' position and the galvanometer key K kept open, the battery supplies the working current through the rheostat and the slide wire. The working current through the slide wire may be varied by changing the rheostat setting.



- The method of measuring the unknown voltage, E1, depends upon the finding a position for the sliding contact such that the galvanometer shows zero deflection, i.e., indicates null condition, when the galvanometer key K is closed.
- Zero galvanometer deflection means that the unknown voltage E1 is equal to the voltage drop E2, across position a—c of the slide wire. Thus, determination of the values of unknown voltage now becomes a matter of evaluating the voltage drop E2 along the portion a—c of the slide wire.

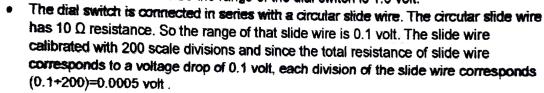
 When the switch S is placed at 'calibrate' position, a standard or reference cell is connected to the circuit. This reference cell is used to standardize the potentiometer.

# Laboratory-Type CROMPTON'S DC POTENTIOMETER:-

Basic slide wire dc potentiometer has the following disadvantages.

- The slide wire is linear and hence occupies more space which is not practical.
- If the length is decreased then resolution of the potentiometer decreases as voltage per unit length increases.
- So Crompton potentiometer is used in practice to decrease the size without compromising the resolution (smallest measurable voltage).
- It consists of a dial switch which has fifteen (or more) steps. Each steep has 10  $\Omega$  resistance. So the dial switch has total 150  $\Omega$  resistance.
- The working current of this potentiometer is 10 mA and therefore each step of the dial switch

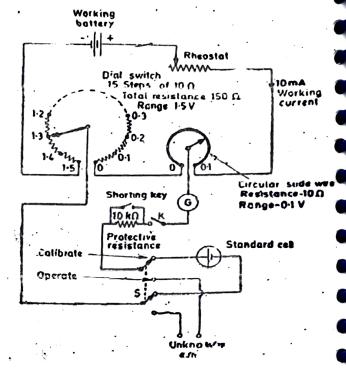
corresponds to 0.1 volt. So the range of the dial switch is 1.5 volt.



With this Crompton's potentiometer it is possible to estimate the reading up to 0,0001
volt.

## Procedure for Measurement of Unknown emf :-

- At first, the combination of the dial switch and the slide wire is set to the standard cell voltage. Let the standard sell voltage be 1.0175 volts, then the dial resistor is put in 1.0 volt and the slide wire at 0.0175 volts setting.
- The switch 'S' is thrown to the calibrate position and the galvanometer switch 'K' is pressed until the rheostat is adjusted for zero deflection on the galvanometer.
- The 10 kW protective resistance is kept in the circuit in the initial stages so as to protect the galvanometer from overload.
- After the null deflection on the galvanometer is approached the protective resistance is shorted so as to increase the sensitivity of the galvanometer. Final adjustment is made for the zero deflection with the help of the rheostat. This completes the standardisation process of the potentiometer.



- After completion of the standardisation, the switch 'S' is thrown to the operate
  position thereby connecting the unknown emf into the potentiometer circuit. With the
  protective resistance in the circuit, the potentiometer is balanced by means of the
  main dial and the slide wire adjustment.
- As soon as the balanced is approached, the protective resistance is shorted and final adjustments are made to obtain true balance.
- After the final true balance is obtained, the value of the unknown emf is read off directly from the setting of the dial switch and the slide wire.
- The standardisation of the potentiometer is checked again by returning the switch 'S'
  to the calibrate position. The dial setting is kept exactly the same as in the original
  standardisation process. If the new reading does not agree with the old one, a
  second measurement of unknown emi must be made. The standardisation again
  should be made after the measurement.

### **AC POTENTIOMETER:**

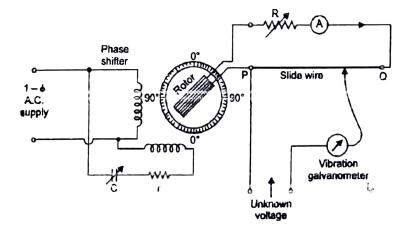
An ac potentiometer is same as dc potentiometer by principle. Only the main difference between the ac and dc potentiometer is that, in case of dc potentiometer, only the magnitude of the unknown emf is compared with the standard cell emf, but in ac potentiometer, the magnitude as well as phase angle of the unknown voltage is compared to achieve balance.

The following points need to be considered for the satisfactory operation of the ac potentiometer:

- To avoid error in reading, the slide wire and the resistance coil of an ac potentiometer should be non-inductive.
- The reading is affected by stray or external magnetic field, so in the time of measurement they must be eliminated or measured and corresponding correction factor should be introduced.
- The sources of ac supply should be free from harmonics, because in presence of harmonics the balance may not be achieved.
- The ac source should be as sinusoidal as possible.

# **Drysdale Polar Potentiometer:**

- The slide wire S1–S2 is supplied from a phase shifting circuit for ac measurement.
- The phase shifting circuit is so arranged that the magnitude of the voltage supplied by it remains constant while its phase can be varied through 360°. Consequently, slide wire current can be maintained constant in magnitude but varied in phase.



- The phase shifting circuit consists of two stator coils connected in parallel supplied from the same source; their currents are made to differ by 90° by using very accurate phase shifting technique.
- The two windings produce rotating flux which induces a secondary emf in the rotor winding which is of constant magnitude but the phase of which can be varied by rotating the rotor in any position. The phase of the rotor emf is read from the circular dial attached in the potentiometer.
- Before the ac measurement, the potentiometer is first calibrated by using dc supply
  for slide wire and standard cell for test terminals T1 and T2. The unknown alternating
  voltage to be measured is applied across test terminals and the balance is achieved
  by varying the slide wire contact and the position of the rotor.
- The ammeter connected in the slide wire circuit gives the magnitude of the unknown emf and the circular dial in the rotor circuit gives the phase angle of it.

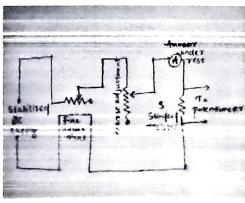
## **APPLICATIONS OF dc POTENTIOMETERS**

Practical uses of dc potentiometers are

- Measurement of current
- Measurement of high voltage
- Measurement of resistance
- · Measurement of power
- Calibration of voltmeter
- · Calibration of ammeter
- Calibration of wattmeter

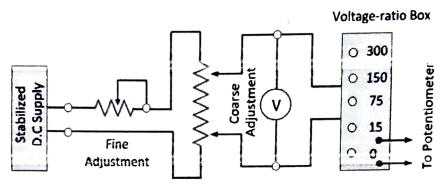
#### Calibration of Ammeter by Potentiometer :-

- Now, compare the reading of the ammeter with the current found by calculation. If they do not match, a positive or negative error will be induced.
- A calibration curve may be drawn between the ammeter reading and the true value of the current as indicated by the potentiometer reading.
- As the resistance of the standard resistor S is exactly known, the current through S is
  exactly calculated. This method of calibration of ammeter is very accurate.



#### Calibration of Voltmeter by Potentiometer :-

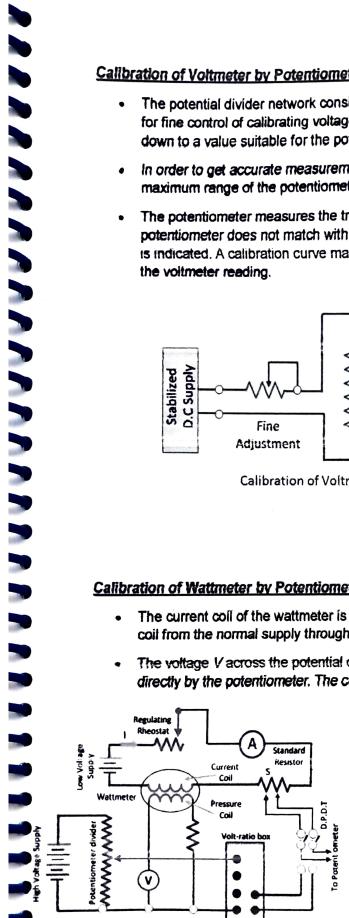
- The potential divider network consists of two rheostats. One for coarse and the other for fine control of calibrating voltage. The voltage across the voltmeter is steeped down to a value suitable for the potentiometer with the help of the volt-ratio box.
- In order to get accurate measurements, it is necessary to measure voltages near the maximum range of the potentiometer, as far as possible.
- The potentiometer measures the true value of the voltage. If the reading of the potentiometer does not match with the voltmeter reading, a positive or negative error is indicated. A calibration curve may be drawn with the help of the potentiometer and the voltmeter reading.



Calibration of Voltmeter with Potentiometer

#### Calibration of Wattmeter by Potentiometer :-

- The current coil of the wattmeter is supplied from low voltage supply and the potential coil from the normal supply through the potential divider.
- The voltage V across the potential coil of the wattmeter under calibration is measured directly by the potentiometer. The current through the current coil is measured by



Calibration of Wattmeter with a DC Pontentioemter

measuring the voltage across a standard resistor connected in series with the current coil divided by the value of the standard resistor.

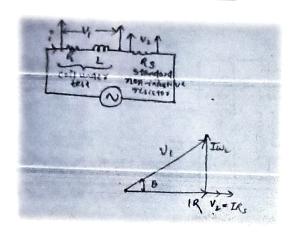
The true power is then VI, where V is the voltage across the potential coil and / is the current through the current coil of the wattmeter. The wattmeter reading may be compared with this value, and a calibration curve may be drawn.

#### **APPLICATIONS OF AC POTENTIOMETER:**

The major applications of the ac potentiometers are

- 1. Measurement of self-inductance
- 2. Calibration of voltmeter
- 3. Calibration of ammeter
- 4. Calibration of wattmeter

# Measurement of Self-Inductance :-



 $I = \frac{V_2}{R_c}$ Or.

Voltage drop across inductive coil =  $V_1$ 

through the coil =  $\theta$  5  $\theta$  6  $\frac{l_s V_l \cos \theta}{V_2}$   $\theta$  6  $\frac{R_s V_l \sin \theta}{V_2 \omega}$  former and the mary is supplied Phase angle between voltage across and current through the coil =  $\theta$ Voltage drop due to resistance of coil,  $IR = V_1 \cos \theta$ 

$$\therefore \text{ resistance of the coil, } R = \frac{V_1 \cos \theta}{I} = \frac{V_1 \cos \theta}{\frac{V_2}{R_S}} = \frac{R_S V_1 \cos \theta}{V_2}$$

Voltage drop due to inductance of  $\infty il$ ,  $I\omega L = V_1 \sin \theta$ 

: inductance of the coil, 
$$L = \frac{V_1 \sin \theta}{I \omega} = \frac{V_1 \sin \theta}{\omega \left(\frac{V_2}{R_S}\right)} = \frac{R_S V_1 \sin \theta}{V_2 \omega}$$

# Calibration of Wattmeter:

The current coil of the wattmeter is supplied through stepdown transformer and the potential coil from the secondary of a variable transformer whose primary is supplied from the rotor of a phase shifting transformer.

- The voltage V across the potential coil of the wattmeter and the current / through the
  current coil of wattmeter are measured by the potentiometer, introducing a volt-ratio
  box and a standard resistor.
- The power factor cos q is varied by rotating the phase shift rotor, the phase angle between voltage and current, F being given by the reading on the dial of the phase shifter.
- The power is then VI cos F and the wattmeter reading may be compared with this
  reading.
- A calibration curve may be drawn if necessary. A small mutual inductance M is included to ensure accuracy of measurement of zero power factor.

### **AC POTENTIOMETER**

#### **Advantages**

- 1. An ac potentiometer is a very versatile instrument. By using shunt and volt-ratio box, it can measure wide range of voltage, current and resistances.
- 2. As it is able to measure phase as well as magnitude of two signals, it is used to measure power, inductance and phase angle of a coil, etc.
- The principle of ac potentiometer is also incorporated in certain special application like Amold circuit for the measurement of CT (Current Transformer) errors.

#### **Disadvantages**

- 1. A small difference in reading of the dynamometer instrument either in dc or ac calibration brings on error in the alternating current to be set at standard value.
- 2. The normal value of the mutual inductance M is affected due to the introduction of mutual inductances of various potentiometer parts and so a slight difference is observed in the magnitude of the current of quadrature wire with compared to that in the in-phase potentiometer wire.
- 3. Inaccuracy in the measured value of frequency will also result in the quadrature potentiometer wire current to differ from that of in-phase potentiometer wire.

# PYO'S ASKED IN MID & END SEMESTER EXAMINATIONS **MODULE IV**

#### **2MARKERS**

- 1) Draw the phasor diagram of current transformer.
- 2) Why the secondary of CT is never kept open ?

#### **4MARKERS**

- 1) What is the role of current transformer? Derive the expression for turns ratio error and phase angle error of CT?
- 2) Derive the expression for turns ratio error and phase angle error of PT?
- 3) Why Potentiometer is used? Explain the working of Crompton potentiometer.
- 4) Differentiate between AC and DC potentiometer.

# NUMERICALS (teacher special)

1) A CT has one turn primary and 200 turns secondary windings . The secondary carries a current of 5 A passing through a secondary burden of 1 ohm . The flux is set up in the core by the current of 80 A. The frequency is 50 Hz and area of cross section is 1000 sq-mm. calculate the actual transformation ratio and phase angle for the transformer.