

NorthWoods Software**Program Name:** Weld-Group_C2**Project Number:** -**Project Description:** -**Project Designer:** Dik**Last Revised (yy-mm-dd):** 21.10.31**Reference:** NBCC, CSA S16**Disclaimer:**

Created using SMath Studio, a MathCAD workalike from <https://en.smath.info/view/SMathStudio>. The User is responsible to verify data and calculations using an alternative method

Menu:

 Input Data	 Important Output	 Logical Constructs	 Blue Units
 Sum / For	 Red Important Note	 Temporary Variables	

Defined Units:

$$\text{grav} := 9.80665 \frac{\text{m}}{\text{sec}^2}$$

$$\text{K} := \text{kip}$$

$$\text{K_ft} := \text{K ft}$$

$$\text{kN_m} := \text{kN m}$$

$$\text{K_in} := \text{K in}$$

$$\text{kN_mm} := \text{kN mm} \quad \text{lb_in} := \text{lbf in}$$

$$\text{kNmpm} := \frac{\text{kN m}}{\text{m}} \quad \text{iKpi} := \frac{\text{K in}}{\text{in}}$$

$$\text{pcf} := \frac{\text{lbf}}{\text{ft}^3}$$

$$\text{kNpcm} := \frac{\text{kN}}{\text{m}^3}$$

$$\text{kgpcm} := \frac{\text{kg}}{\text{m}^3}$$

$$\text{Klf} := \frac{\text{K}}{\text{ft}}$$

$$\text{plf} := \frac{\text{lbf}}{\text{ft}}$$

$$\text{kNpm} := \frac{\text{kN}}{\text{m}}$$

$$\text{Kpi} := \frac{\text{K}}{\text{in}}$$

$$\text{kNpmm} := \frac{\text{kN}}{\text{mm}}$$

$$\text{psf} := \frac{\text{lbf}}{\text{ft}^2}$$

$$\text{Ksf} := \frac{\text{K}}{\text{ft}^2}$$

$$\text{Ksi} := \frac{\text{K}}{\text{in}^2}$$

$$\text{kNpsm} := \frac{\text{kN}}{\text{m}^2}$$

$$\text{psi} := \frac{\text{lbf}}{\text{in}^2}$$

$$\text{Npsmm} := \frac{\text{N}}{\text{mm}^2}$$

$$\text{pci} := \frac{\text{lbf}}{\text{in}^3}$$

$$\text{psf pf} := \frac{\text{psf}}{\text{ft}}$$

$$\text{kPapm} := \frac{\text{kPa}}{\text{m}}$$

$$\text{pmcf} := \frac{\text{lb}}{\text{ft}^3}$$

$$\text{lb} := \text{lbf}$$

$$\text{mph} := \frac{\text{mi}}{\text{hr}}$$

$$\text{kph} := \frac{\text{km}}{\text{hr}}$$

$$\text{mps} := \frac{\text{m}}{\text{sec}}$$

$$\text{ispf} := \frac{\text{in}^2}{\text{ft}}$$

$$\text{mmspm} := \frac{\text{mm}^2}{\text{m}}$$

$$\text{ppf} := \frac{\text{lbf}}{\text{ft}}$$

$$\text{Npm} := \frac{\text{N}}{\text{m}}$$

Acceleration

Force

Moment

Moment per Unit Length

Density

Force/Unit Length

Pressure

Pressure

Subgrade Modulus

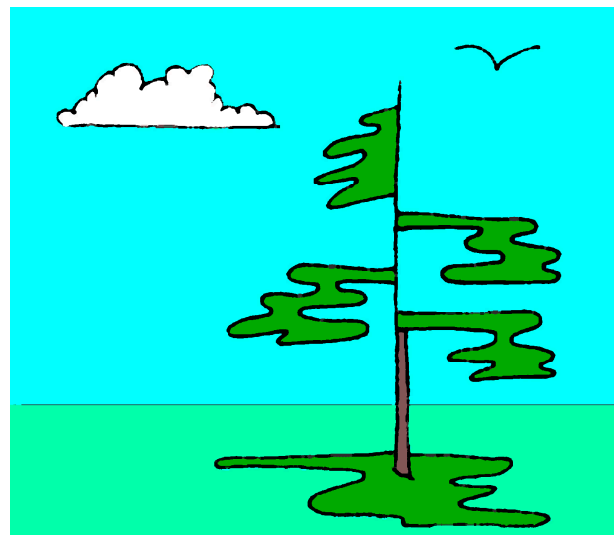
Pressure per Depth

Force

Velocity/Speed

Area per Unit Length

Stiffness



Input Data**Material Property Factors:**

$$\phi_s := 0.90$$

$$\phi_w := 0.67$$

Load Factors:

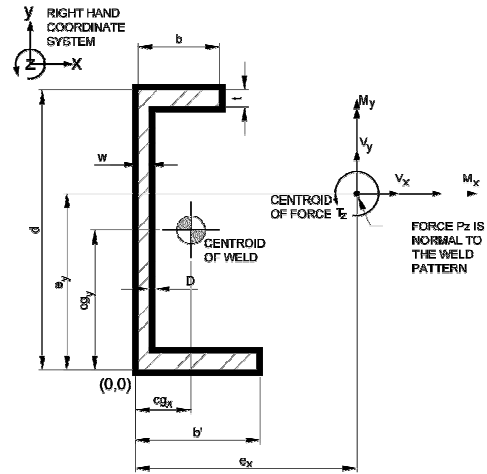
$$\alpha_L := 1.50$$

$$\alpha_D := 1.25$$

$$\text{Check}(\alpha_D \geq 1.25) = "...OK"$$

$$\text{Check}(\alpha_L \geq 1.5) = "...OK"$$

Weld interface is taken at the face of the attached member rather than the centreline of the weld.

**Applied Factored Loads:**

$$P_{fz} := 0 \text{ kN}$$

$$V_{fx} := 0 \text{ kN}$$

$$V_{fy} := 0 \text{ kN}$$

$$M_{fx} := 0 \text{ kN}_m$$

$$M_{fy} := 0 \text{ kN}_m$$

$$T_{fz} := 14 \text{ kN}_m$$

Load Eccentricity:

$$e_x := 3 \text{ in}$$

$$e_y := 5 \text{ in}$$

$$e_z := 0 \text{ in}$$

C Shape Input Data:

$$d := 10 \text{ in}$$

$$b := 1 \text{ in}$$

$$b' := 2.6 \text{ in}$$

$$t := .436 \text{ in}$$

$$w := .24 \text{ in}$$

$$P_{fz} = 0.00 \text{ kN}$$

Axial Load

$$V_{fx} = 0.00 \text{ kN}$$

Shear (X-Axis)

$$V_{fy} = 0.00 \text{ kN}$$

Shear (Y-Axis)

$$M_{fx} = 0 \text{ kN}_m$$

Moment (X-Axis)

$$M_{fy} = 0.00 \text{ kN}_m$$

Moment (Y-Axis)

$$T_{fz} = 18.98 \text{ kN}_m$$

Torsion (Z-Axis)

$$e_x = 76.2 \text{ mm}$$

Eccentricity X-Axis Direction

$$e_y = 127 \text{ mm}$$

Eccentricity Y-Axis Direction

$$e_z = 0.0 \text{ mm}$$

Eccentricity Z-Axis Direction

$$d = 254 \text{ mm}$$

Depth of Channel Section

$$b = 25.4 \text{ mm}$$

Width of Top Flange

$$b' = 66 \text{ mm}$$

Width of Bottom Flange

$$t = 11.1 \text{ mm}$$

Thickness of Flange

$$w = 6.1 \text{ mm}$$

Thickness of Web

$$pts := \begin{bmatrix} s & x_i & y_i & x_j & y_j \\ 1 & 0 \text{ in} & 0 \text{ in} & 0 \text{ in} & d \\ 2 & 0 \text{ in} & d & b & d \\ 3 & b & d & b & d-t \\ 4 & b & d-t & w & d-t \\ 5 & w & d-t & w & t \\ 6 & w & t & b' & t \\ 7 & b' & t & b' & 0 \text{ in} \\ 8 & b' & 0 \text{ in} & 0 \text{ in} & 0 \text{ in} \end{bmatrix}$$

$$pts' := \text{submatrix}(pts, 1, \text{rows}(pts), 2, 5)$$

Used for Summary and Plotting Shape

$$\text{for } c \in [1..rows(pts')] \\ ptsn_{c1} := pts'_{c1} \cdot \frac{1}{in} \\ ptsn_{c2} := pts'_{c2} \cdot \frac{1}{in} \\ ptsn_{c3} := pts'_{c3} \cdot \frac{1}{in} \\ ptsn_{c4} := pts'_{c4} \cdot \frac{1}{in}$$

$c := 0$

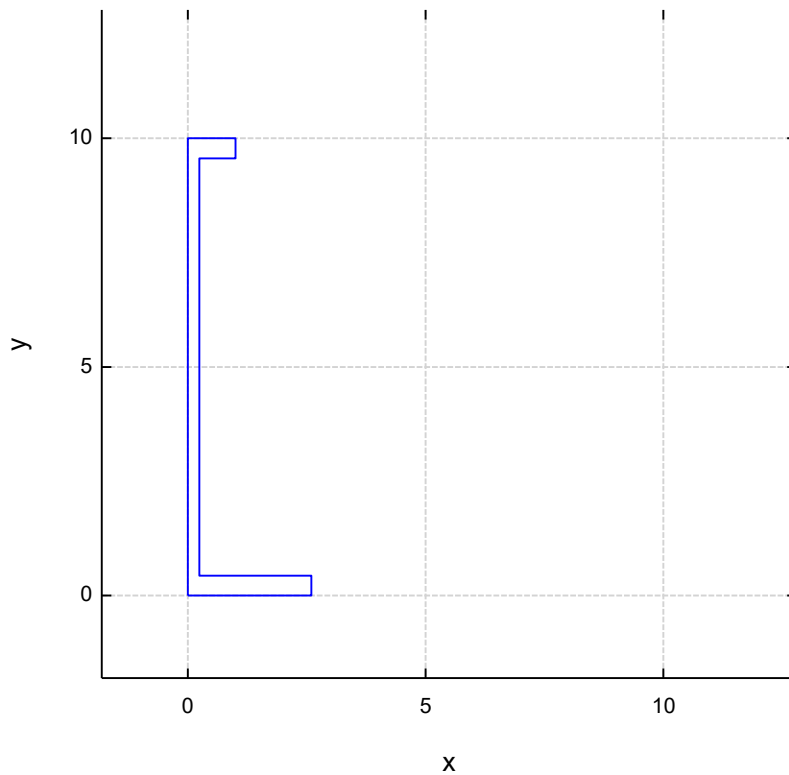
```
for c ∈ [1..rows(ptsn)]
  weld c 1 := ptsn c 1
  weld c 2 := ptsn c 2
```

$c := c + 1$

$weld_{c 1} := ptsn_{1 1}$

$weld_{c 2} := ptsn_{1 2}$

Weld Pattern (Adjust Size as Required)



$weld$

Steel Properties:

Part: $st_{NDX} := 1$

NDX	des	fy	Fu
1	"G40.21-350W"	50 Ksi	65 Ksi
2	"G40.21-300W"	44 Ksi	65 Ksi
3	"A36"	36 Ksi	58 Ksi

$desM_1 := st_{NDX 2}$ $f_{y1} := st_{NDX 3}$ $F_{u1} := st_{NDX 4}$
 $G_s := \frac{E_s}{2 \cdot (1 + \nu)}$ $\gamma_s := 489 \text{ pcf}$ $\nu := 0.3$ $E_s := 29000 \text{ Ksi}$

Base: $st_{NDX} := 2$

$desM_2 := st_{NDX 2}$ $f_{y2} := st_{NDX 3}$ $F_{u2} := st_{NDX 4}$

Weld Design:

Weld Electrodes: $we_{NDX} := 2$

NDX	Desl	DesM	UTS
1	"E60xx"	"E43xx"	60 ksi
2	"E70xx"	"E49xx"	70 ksi
3	"E80xx"	"E55xx-x"	80 ksi
4	"E90xx"	"E62xx-x"	90 ksi

$desI_w := we_{NDX 2}$ $desM_w := we_{NDX 3}$ $X_u := we_{NDX 4}$

Weld Sizes: $ws_{NDX} := 13$

	NDX	desl	desM	D	
$ws :=$	1	""	"3mm"	0.11811 in	$desI_D := ws_{ws_{NDX} 2}$
	2	"1/8"	""	0.125 in	$desM_D := ws_{ws_{NDX} 3}$
	3	""	"4mm"	0.15748 in	$D := ws_{ws_{NDX} 4}$
	4	"3/16"	""	0.1875 in	
	5	""	"5mm"	0.19685 in	
	6	""	"6mm"	0.23622 in	
	7	"1/4"	""	0.25 in	
	8	""	"7mm"	0.275591 in	
	9	"5/16"	""	0.3125 in	
	10	""	"8mm"	0.314961 in	
	11	""	"9mm"	0.354331 in	
	12	"3/8"	""	0.375 in	
	13	""	"10mm"	0.3937 in	
	14	""	"11mm"	0.4331 in	
	15	"7/16"	""	0.4375 in	
	16	""	"12mm"	0.4724 in	
	17	"1/2"	""	0.50 in	

Weld Material Strength

$$v_{rw} := \phi_w \cdot 0.67 \cdot X_u \cdot \frac{1}{\sqrt{2}} \quad v_{rw} = 22.2 \text{ ksi} \quad v_{rw} = 153.2 \text{ MPa}$$

Part Metal Strength

$$v_{rb1} := \phi_w \cdot 0.67 \cdot F_{u1} \quad v_{rb1} = 29.2 \text{ Ksi} \quad v_{rb1} = 201.2 \text{ MPa}$$

Base Metal Strength

$$v_{rb2} := \phi_w \cdot 0.67 \cdot F_{u1} \quad v_{rb2} = 29.2 \text{ Ksi} \quad v_{rb2} = 201.2 \text{ MPa}$$

Minimum Weld Capacity

$$V_{rw} := \min \left(\left[v_{rw} \quad v_{rb1} \quad v_{rb2} \right] \right) \quad V_{rw} = 22.2 \text{ Ksi} \quad V_{rw} = 153.2 \text{ MPa}$$

Weld Properties:

```

for r ∈ [1..rows(pts)]
  pts_r6 := (pts_r2 + pts_r4) / 2
  pts_r7 := (pts_r3 + pts_r5) / 2
  pts_r8 := pts_r4 - pts_r2
  pts_r9 := pts_r5 - pts_r3
  pts_r10 := sqrt((pts_r8)^2 + (pts_r9)^2)
  pts_r11 := (pts_r10 * (pts_r9)^2) / 12
  pts_r12 := (pts_r10 * (pts_r8)^2) / 12
  pts_r13 := pts_r10 * pts_r6
  pts_r14 := pts_r10 * pts_r7

```

c_x
 c_y
 m
 n
 L
 I_{xx}
 I_{yy}
 L_{cx}
 L_{cy}

```

for r ∈ [1..rows(pts)]
  ptsr 15 := ptsr 6 - cgx
  ptsr 16 := ptsr 7 - cgy
  ptsr 17 := ptsr 11 + ptsr 10 · ptsr 162
  ptsr 18 := ptsr 12 + ptsr 10 · (ptsr 15)2
  ptsr 19 := ptsr 10 · ptsr 15 · ptsr 16
  ptsr 20 := ptsr 2 - cgx
  ptsr 21 := ptsr 3 - cgy
  ptsr 22 := ptsr 4 - cgx
  ptsr 23 := ptsr 5 - cgy

```

 d_x d_y I'_{xx} I'_{yy} I'_{xy} d_{xi} d_{yi} d_{xj} d_{yj}

$A := \sum \text{col}(\text{pts}, 10)$	$A = 26.72 \text{ in}$	$A = 678.7 \text{ mm}$	Total Length of Weld
$cg_x := \sum \left(\frac{\text{col}(\text{pts}, 13)}{A} \right)$	$cg_x = 0.43 \text{ in}$	$cg_x = 10.9 \text{ mm}$	Centroid of Weld X-Axis
$cg_y := \sum \left(\frac{\text{col}(\text{pts}, 14)}{A} \right)$	$cg_y = 4.43 \text{ in}$	$cg_y = 112.5 \text{ mm}$	Centroid of Weld Y-Axis
$I'_{xx} := \sum \text{col}(\text{pts}, 17)$	$I'_{xx} = 312.9 \text{ in}^3$	$I'_{xx} = 5.13 \cdot 10^6 \text{ mm}^3$	Moment of Inertia (X-Axis)
$I'_{yy} := \sum \text{col}(\text{pts}, 18)$	$I'_{yy} = 11.4 \text{ in}^3$	$I'_{yy} = 1.86 \cdot 10^5 \text{ mm}^3$	Moment of Inertia (Y-Axis)
$I'_{xy} := \sum \text{col}(\text{pts}, 19)$	$I'_{xy} = -24.3 \text{ in}^3$	$I'_{xy} = -3.98 \cdot 10^5 \text{ mm}^3$	Product of Inertia
$I'_p := I'_{xx} + I'_{yy}$	$I'_p = 324.3 \text{ in}^3$	$I'_p = 5.31 \cdot 10^6 \text{ mm}^3$	Polar Moment of Inertia
$I'_{prod} := I'_{xx} \cdot I'_{yy} - I'_{xy}^2$	$I'_{prod} = 2965.2 \text{ in}^6$	$I'_{prod} = 7.96 \cdot 10^{11} \text{ mm}^6$	Product of Inertia
Load Distance from Centroid:			
$e'_x := e_x - cg_x$	$e'_x = 2.57 \text{ in}$	$e'_x = 65.3036 \text{ mm}$	X-Axis Direction
$e'_y := e_y - cg_y$	$e'_y = 0.57 \text{ in}$	$e'_y = 14.5464 \text{ mm}$	Y-Axis Direction
$e'_z := e_z$	$e'_z = 0.00 \text{ in}$	$e'_z = 0 \text{ mm}$	Z-Axis Direction

Stress from Applied Factored Loads:

$\sigma_{fx} := \frac{V_{fx}}{A}$	$\sigma_{fx} = 0.00 \text{ Kpi}$	$\sigma_{fx} = 0 \text{ kNpmm}$	X-Axis Direction
$\sigma_{fy} := \frac{V_{fy}}{A}$	$\sigma_{fy} = 0 \text{ Kpi}$	$\sigma_{fy} = 0 \text{ kNpmm}$	Y-Axis Direction
$\sigma_{fz} := \frac{P_{fz}}{A}$	$\sigma_{fz} = 0 \text{ Kpi}$	$\sigma_{fz} = 0 \text{ kNpmm}$	Z-Axis Direction

Load at Weld Group Centroid:

$d_x := e_x - cg_x$	$d_x = 2.57 \text{ in}$	$d_x = 65.30 \text{ mm}$
$d_y := e_y - cg_y$	$d_y = 0.5727 \text{ in}$	$d_y = 14.5464 \text{ mm}$
$d_z := e_z$	$d_z = 0 \text{ in}$	$d_z = 0 \text{ mm}$
$M'_{fx} := M_{fx} - V_{fy} \cdot d_z + P_{fz} \cdot d_y$	$M'_{fx} = 0.00 \text{ K_ft}$	$M'_{fx} = 0 \text{ kN_m}$
$M'_{fy} := M_{fy} + V_{fx} \cdot d_z - P_{fz} \cdot d_x$	$M'_{fy} = 0 \text{ K_ft}$	$M'_{fy} = 0 \text{ kN_m}$
$T'_{fz} := T_{fz} - V_{fx} \cdot d_y + V_{fy} \cdot d_x$	$T'_{fz} = 14 \text{ K_ft}$	$T'_{fz} = 18.9815 \text{ kN_m}$

```

for r ∈ [1..rows(pts)]
  if pts_r 10 = 0 in
    pts_r 24 := 0 pli
    pts_r 25 := 0 pli
    pts_r 26 := 0 pli
    pts_r 27 := 0 pli
    pts_r 28 := pts_r 24 + pts_r 25 + pts_r 26 + pts_r 27
    pts_r 29 := pts_r 28 + σfz
    pts_r 30 := 0 pli
    pts_r 31 := pts_r 30 + σfx
    pts_r 32 := 0 pli
    pts_r 33 := pts_r 32 + σfy
    pts_r 34 := √(pts_r 292 + pts_r 312 + pts_r 332)
    pts_r 35 := 0 pli
  else
    pts_r 24 :=  $\frac{pts_{r 21} \cdot M'_{fx} \cdot I'_{yy}}{I'_{prod}}$ 
    pts_r 25 :=  $\frac{pts_{r 21} \cdot M'_{fy} \cdot I'_{xy}}{I'_{prod}}$ 
    pts_r 26 :=  $\frac{(-1 \cdot pts_{r 20}) \cdot M'_{fx} \cdot I'_{xy}}{I'_{prod}}$ 
    pts_r 27 :=  $\frac{(-1 \cdot pts_{r 20}) \cdot M'_{fy} \cdot I'_{xx}}{I'_{prod}}$ 
    pts_r 28 := pts_r 24 + pts_r 25 + pts_r 26 + pts_r 27
    pts_r 29 := pts_r 28 + σfz
    pts_r 30 :=  $\frac{(-1 \cdot pts_{r 21}) \cdot T'_{fz}}{I'_p}$ 
    pts_r 31 := pts_r 30 + σfx
    pts_r 32 :=  $\frac{pts_{r 20} \cdot T'_{fz}}{I'_p}$ 
    pts_r 33 := pts_r 32 + σfy
    pts_r 34 := √((pts_r 29)2 + (pts_r 31)2 + (pts_r 33)2)
    pts_r 35 :=  $\frac{pts_{r 23} \cdot M'_{fx} \cdot I'_{yy}}{I'_{prod}}$ 

```

σ_z y from M_x Stress at Start of Segmentσ_z y from M_yσ_z x from M_xσ_z x from M_yΣσ_z from MΣσ_zσ_x from TΣσ_xσ_y from TΣσ_yσ_y combinedσ_z y from M_xσ_z y from M_yσ_z x from M_xσ_z x from M_yΣσ_z from MΣσ_zσ_x from TΣσ_xσ_y from TΣσ_yσ_y combinedΣσ_y

Stress at Start of Segment

σ_z y from M_x

Stress at End of Segment

```
for r ∈ [1..rows(pts)]
```

```
  if ptsr 10 = 0 in
```

```
    ptsr 36 := 0 pli
```

```
    ptsr 37 := 0 pli
```

```
    ptsr 38 := 0 pli
```

```
    ptsr 39 := ptsr 35 + ptsr 36 + ptsr 37 + ptsr 38
```

```
    ptsr 40 := (ptsr 39 +  $\sigma_{fz}$ )
```

```
    ptsr 41 := 0 pli
```

```
    ptsr 42 := ptsr 41 +  $\sigma_{fx}$ 
```

```
    ptsr 43 := 0 pli
```

```
    ptsr 44 := ptsr 43 +  $\sigma_{fy}$ 
```

```
    ptsr 45 :=  $\sqrt{(pts_{r 40})^2 + (pts_{r 42})^2 + (pts_{r 44})^2}$ 
```

```
    ptsr 46 := 0 pli
```

```
    ptsr 47 := 0 pli
```

```
    ptsr 48 := 0 pli
```

```
  else
```

```
    ptsr 36 :=  $\frac{pts_{r 23} \cdot M'_{fy} \cdot I'_{xy}}{I'_{prod}}$ 
```

```
    ptsr 37 :=  $\frac{(-1 \cdot pts_{r 22}) \cdot M'_{fx} \cdot I'_{xy}}{I'_{prod}}$ 
```

```
    ptsr 38 :=  $\frac{(-1 \cdot pts_{r 22}) \cdot M'_{fy} \cdot I'_{xx}}{I'_{prod}}$ 
```

```
    ptsr 39 := ptsr 35 + ptsr 36 + ptsr 37 + ptsr 38
```

```
    ptsr 40 := (ptsr 39 +  $\sigma_{fz}$ )
```

```
    ptsr 41 :=  $\left( -\frac{1 \cdot pts_{r 23} \cdot T'_{fz}}{I'_p} \right)$ 
```

```
    ptsr 42 := ptsr 41 +  $\sigma_{fx}$ 
```

```
    ptsr 43 :=  $\frac{pts_{r 22} \cdot T'_{fz}}{I'_p}$ 
```

```
    ptsr 44 := ptsr 43 +  $\sigma_{fy}$ 
```

```
    ptsr 45 :=  $\sqrt{(pts_{r 40})^2 + (pts_{r 42})^2 + (pts_{r 44})^2}$ 
```

```
    ptsr 46 :=  $\frac{pts_{r 16} \cdot M'_{fx} \cdot I'_{yy}}{I'_{prod}}$ 
```

```
    ptsr 47 :=  $\frac{pts_{r 16} \cdot M'_{fy} \cdot I'_{xy}}{I'_{prod}}$ 
```

```
    ptsr 48 :=  $\frac{(-1 \cdot pts_{r 15} \cdot M'_{fx} \cdot I'_{xy})}{I'_{prod}}$ 
```

σ_z y from My

σ_z x from Mx

σ_z x from My

$\Sigma \sigma_z$ from M

$\Sigma \sigma_z$

σ_x from T

$\Sigma \sigma_x$

σ_y from T

$\Sigma \sigma_y$

σ_y combined

σ_z y from Mx

σ_z y from My

σ_z x from Mx

σ_z y from My

σ_z x from Mx

σ_z x from My

$\Sigma \sigma_z$ from M

$\Sigma \sigma_z$

σ_x from T

$\Sigma \sigma_x$

σ_y from T

$\Sigma \sigma_y$

σ_y combined

Stress at End of Segment

σ_z y from Mx

Stress at Midpoint of Segment

σ_z y from My

<pre> for r ∈ [1..rows(pts)] if pts_r 10 = 0 in pts_r 49 := 0 pli pts_r 50 := pts_r 46 + pts_r 47 + pts_r 48 + pts_r 49 pts_r 51 := pts_r 50 + σ_{fz} pts_r 52 := 0 pli pts_r 53 := pts_r 52 · σ_{fx} pts_r 54 := 0 pli pts_r 55 := pts_r 54 + σ_{fy} pts_r 56 := √((pts_r 51)² + (pts_r 53)² + (pts_r 55)²) else pts_r 49 := $\frac{(-1 \cdot pts_r 15) \cdot M'_{fy} \cdot I'_{xx}}{I'_{prod}}$ pts_r 50 := pts_r 46 + pts_r 47 + pts_r 48 + pts_r 49 pts_r 51 := pts_r 50 + σ_{fz} pts_r 52 := $\frac{(-1 \cdot pts_r 16) \cdot T'_{fz}}{I'_p}$ pts_r 53 := (pts_r 52 + σ_{fx}) pts_r 54 := $\frac{pts_r 15 \cdot T'_{fz}}{I'_p}$ pts_r 55 := pts_r 54 + σ_{fy} pts_r 56 := √((pts_r 51)² + (pts_r 53)² + (pts_r 55)²) </pre>		σ _z x from M _x
		σ _z x from M _y
		σ _z frin M
		σ _z Total
		σ _x from T
		σ _x Combined
		σ _y from T
		σ _y Combined
		Total σ
		σ _z x from M _y
		σ _z frin M
		σ _z Total
		σ _x from T
		σ _x Combined
		σ _y from T
		σ _y Combined
		Total σ
		Stress at Midpoint of Segment

Max and Min Stress in Segment:

$\sigma'_z := \max(\text{col}(\text{pts}, 34))$	$\sigma'_z = 2.90 \text{ Kpi}$	$\sigma'_z = 0.51 \text{ kNpmm}$	Max Stress at Start of Segment
$op'_1 := \min(\text{col}(\text{pts}, 34))$	$op'_1 = 2 \text{ Kpi}$	$op'_1 = 0 \text{ kNpmm}$	Min Stress at Start of Segment
$\sigma'_x := \max(\text{col}(\text{pts}, 45))$	$\sigma'_x = 2.9 \text{ Kpi}$	$\sigma'_x = 0.51 \text{ kNpmm}$	Max Stress at End of Segment
$op'_2 := \min(\text{col}(\text{pts}, 45))$	$op'_2 = 2.0702 \text{ Kpi}$	$op'_2 = 0.3626 \text{ kNpmm}$	Min Stress at End of Segment
$\sigma'_y := \max(\text{col}(\text{pts}, 56))$	$\sigma'_y = 2.89 \text{ Kpi}$	$\sigma'_y = 0.51 \text{ kNpmm}$	Max Stress at Middle of Segment
$op'_3 := \min(\text{col}(\text{pts}, 56))$	$op'_3 = 0.3125 \text{ Kpi}$	$op'_3 = 0.0547 \text{ kNpmm}$	Min Stress at Middle of Segment

Max and Min Stress in Welds:

$op_{max} := \max([\sigma'_x \ \sigma'_y \ \sigma'_z])$	$op_{max} = 2.9 \text{ Kpi}$	$op_{max} = 0.51 \text{ kNpmm}$	Maximum Stress in Segment
$op'_{min} := \min([op'_1 \ op'_2 \ op'_3])$	$op'_{min} = 0.3125 \text{ Kpi}$	$op'_{min} = 0.0547 \text{ kNpmm}$	Minimum Stress in Segment
$v_r := v_{rw} \cdot D$	$v_r = 8.75 \text{ Kpi}$	$v_r = 1.532 \text{ kNpmm}$	Weld Resistance per Unit Length

Check ($v_r \geq op_{max}$) = "...OK"

Check ($v_r \geq 0.95 \cdot op_{max}$) = "...OK"

c

b

a

Summary:**Material Property Factors**

$$\text{Rolled Sections } \phi_s = 0.9$$

$$\text{Weld } \phi_w = 0.67$$

$$\text{Dead Load Factor } \alpha_D = 1.25$$

$$\text{Live Load Factor } \alpha_L = 1.5$$

$$\text{Check } (\alpha_D \geq 1.25) = "...OK"$$

$$\text{Check } (\alpha_L \geq 1.5) = "...OK"$$

Applied Factored Loads:

Axial Load

Shear (X-Axis)

Shear (Y-Axis)

Moment (X-Axis)

Moment (Y-Axis)

Torsion (Z-Axis)

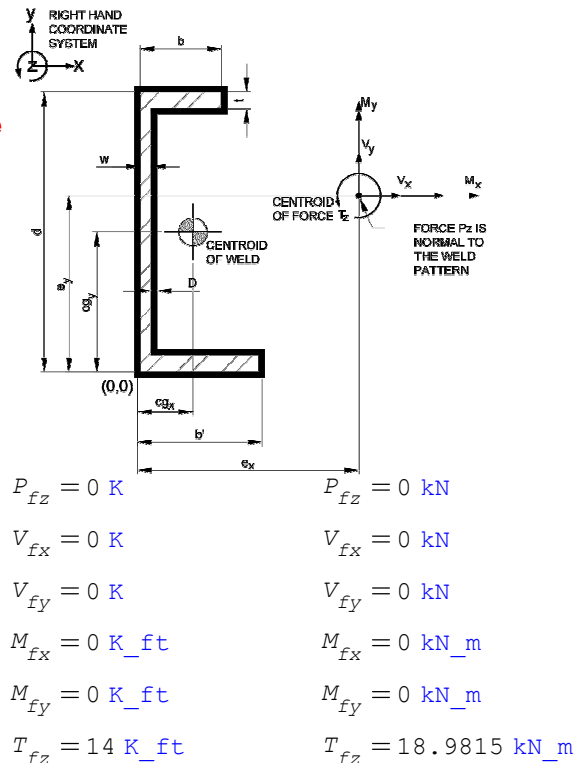
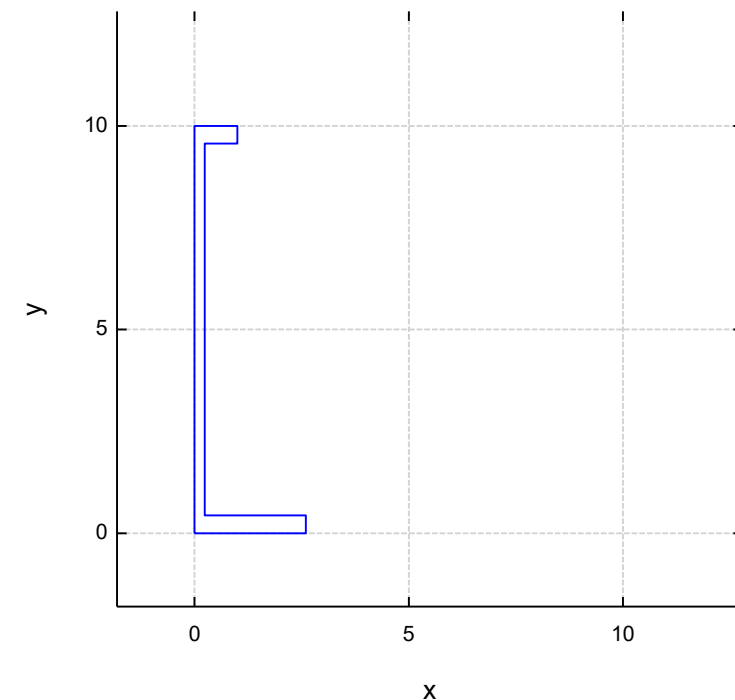
Load Eccentricity from Origin:

X-Axis Direction

Y-Axis Direction

Z-Axis Direction

Weld interface is taken at the face of the attached member rather than the centreline of the weld.

**Weld Pattern**

weld

Segment Input Data:

Row Represents Segment
Number Columns represent
 $S(x_i, y_i, x_j, y_j)$ coordinates

$$pts' = \begin{bmatrix} 0.0 & 0.0 & 0.0 & 10.0 \\ 0.0 & 10.0 & 1.0 & 10.0 \\ 1.0 & 10.0 & 1.0 & 9.6 \\ 1.0 & 9.6 & 0.2 & 9.6 \\ 0.2 & 9.6 & 0.2 & 0.4 \\ 0.2 & 0.4 & 2.6 & 0.4 \\ 2.6 & 0.4 & 2.6 & 0.0 \\ 2.6 & 0.0 & 0.0 & 0.0 \end{bmatrix} \text{ in}$$

$$pts' = \begin{bmatrix} 0 & 0 & 0 & 254 \\ 0 & 254 & 25.4 & 254 \\ 25.4 & 254 & 25.4 & 242.9 \\ 25.4 & 242.9 & 6.1 & 242.9 \\ 6.1 & 242.9 & 6.1 & 11.1 \\ 6.1 & 11.1 & 66 & 11.1 \\ 66 & 11.1 & 66 & 0 \\ 66 & 0 & 0 & 0 \end{bmatrix} \text{ mm}$$

Steel Base Properties**Part**

Designation

$$desM_1 = \text{"G40.21-350W"}$$

Yield Strength

$$f_{y1} = 50 \text{ Ksi}$$

$$f_{y1} = 345 \text{ MPa}$$

Ultimate Strength

$$F_{u1} = 65 \text{ Ksi}$$

$$F_{u1} = 448 \text{ MPa}$$

Base

Designation

$$desM_2 = \text{"G40.21-300W"}$$

Yield Strength

$$f_{y2} = 44 \text{ Ksi}$$

$$f_{y2} = 303 \text{ MPa}$$

Ultimate Strength

$$F_{u2} = 65 \text{ Ksi}$$

$$F_{u2} = 448 \text{ MPa}$$

Young's Modulus

$$E_s = 29000 \text{ Ksi}$$

$$E_s = 1.9995 \cdot 10^5 \text{ MPa}$$

Shear Modulus

$$G_s = 11153.8462 \text{ Ksi}$$

$$G_s = 76903 \text{ MPa}$$

Density

$$\gamma_s = 489 \text{ pcf}$$

$$\gamma_s = 76.8158 \text{ kNpcm}$$

Welding Electrodes

Imperial Designation

$$desI_w = \text{"E70xx"}$$

Metric Designation

$$desM_w = \text{"E49xx"}$$

Ultimate Strength

$$X_u = 70 \text{ ksi}$$

$$X_u = 483 \text{ MPa}$$

Weld Size

Imperial Designation

$$desI_D = \text{" "}$$

Metric Designation

$$desM_D = \text{"10mm"}$$

Size

$$D = 0.3937 \text{ in}$$

$$D = 10 \text{ mm}$$

Base Metal Strength

$$v_{rb1} = 29.2 \text{ Ksi}$$

$$v_{rb1} = 201.2 \text{ MPa}$$

Minimum Weld Capacity

$$V_{rw} = 22.2 \text{ Ksi}$$

$$V_{rw} = 153.2 \text{ MPa}$$

Min Resistance per Unit Len

$$v_r = 8.7 \text{ Kpi}$$

$$v_r = 1.5 \text{ kNpmm}$$

Weld Properties

Total Length of Weld

$$A = 26.72 \text{ in}$$

$$A = 678.7 \text{ mm}$$

Centroid of Weld X-Axis

$$cg_x = 0.429 \text{ in}$$

$$cg_x = 10.9 \text{ mm}$$

Centroid of Weld Y-Axis

$$cg_y = 4.4273 \text{ in}$$

$$cg_y = 112.5 \text{ mm}$$

Moment of Inertia (X-Axis)

$$I'_{xx} = 312.9 \text{ in}^3$$

$$I'_{xx} = 5.13 \cdot 10^6 \text{ mm}^3$$

Moment of Inertia (Y-Axis)

$$I'_{yy} = 11.4 \text{ in}^3$$

$$I'_{yy} = 1.86 \cdot 10^5 \text{ mm}^3$$

Product of Inertia

$$I'_{xy} = -24.3 \text{ in}^3$$

$$I'_{xy} = -3.98 \cdot 10^5 \text{ mm}^3$$

Polar Moment of Inertia

$$I'_p = 324.3 \text{ in}^3$$

$$I'_p = 5.31 \cdot 10^6 \text{ mm}^3$$

Prod of Moment of Inertia

$$I'_{prod} = 2965.2 \text{ in}^6$$

$$I'_{prod} = 7.96 \cdot 10^{11} \text{ mm}^6$$

Weld Force from Direct Loads

X-Axis Direction

$$\sigma_{fx} = 0.00 \text{ Kpi}$$

$$\sigma_{fx} = 0.00 \text{ kNpmm}$$

Y-Axis Direction

$$\sigma_{fy} = 0.00 \text{ Kpi}$$

$$\sigma_{fy} = 0.00 \text{ kNpmm}$$

Z-Axis Direction

$$\sigma_{fz} = 0.00 \text{ Kpi}$$

$$\sigma_{fz} = 0.00 \text{ kNpmm}$$

Load at Weld Group Centroid:

Moment (X-Axis)

$M'_{fx} = 0 \text{ K_ft}$

$M'_{fx} = 0 \text{ kN_m}$

Moment (Y-Axis)

$M'_{fy} = 0 \text{ K_ft}$

$M'_{fy} = 0 \text{ kN_m}$

Torsion (Z-Axis)

$T'_{fz} = 14 \text{ K_ft}$

$T'_{fz} = 18.9815 \text{ kN_m}$

Max Weld Force at Start of Segment in Pattern

$\sigma'_x = 2.902 \text{ Kpi}$

$\sigma'_x = 0.51 \text{ kNpmm}$

Min Weld Force at Start of Segment in Pattern

$op'_1 = 2.07 \text{ Kpi}$

$op'_1 = 0 \text{ kNpmm}$

Max Weld Force at End of Segment in Pattern

$\sigma'_y = 2.887 \text{ Kpi}$

$\sigma'_y = 0.51 \text{ kNpmm}$

Min Weld Force at End of Segment in Pattern

$op'_2 = 2.07 \text{ Kpi}$

$op'_2 = 0.36 \text{ kNpmm}$

Max Weld Force at Mid Point of Segment in Pattern

$\sigma'_z = 2.902 \text{ Kpi}$

$\sigma'_z = 0.51 \text{ kNpmm}$

Min Weld Force at Mid Point of Segment in Pattern

$op'_3 = 0.312 \text{ Kpi}$

$op'_3 = 0.05 \text{ kNpmm}$

Maximum Weld Force in Pattern

$op_{max} = 2.902 \text{ Kpi}$

$op_{max} = 0.51 \text{ kNpmm}$

Minimum Weld Force in Pattern

$op'_{min} = 0.312 \text{ Kpi}$

$op'_{min} = 0.05 \text{ kNpmm}$

Weld Resistance:

$v_r = 8.748 \text{ Kpi}$

$v_r = 1.53 \text{ kNpmm}$

$$Check \left(v_r \geq op_{max} \right) = "...OK"$$

$$Check \left(v_r \geq 0.95 \cdot op_{max} \right) = "...OK"$$

$$Check \left(v_r \geq |op'_{min}| \right) = "...OK"$$